

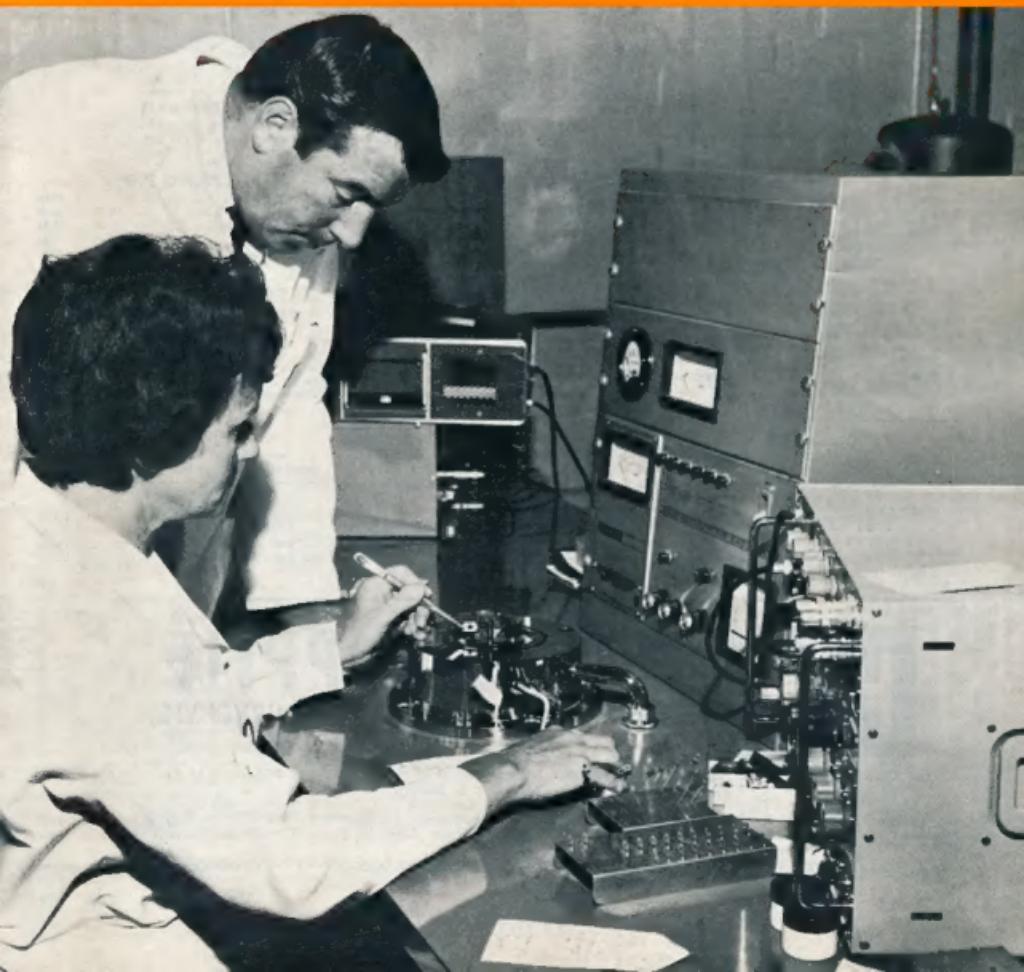
# amateur radio

Vol. 38, No. 11

NOVEMBER, 1970

Registered at G.P.O., Melbourne, for  
transmission by post as a periodical

Price 30 Cents



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### CITIZENS BAND AND MODEL RADIO CONTROL FREQUENCY CRYSTALS

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28.640 MHz.	27.095 MHz.
28.660 MHz.	27.145 MHz.
28.785 MHz.	27.195 MHz.
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HC8 Holders, $\frac{1}{8}$ inch spacing.	
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Channel B	Receive 10,285.71 KHz.
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Channel C	Receive 10,296.14 KHz.
Channel 4	Transmit 4,063.66 KHz.
Channel 4	Receive 10,278.57 KHz.
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2,524 KHz.	2,739 KHz.
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0-1000 mV.	DC Volts: 0-10, 50, 250, 1,000V.
0-10, 50, 250, 1,000V.	AC Volts: 0-2.5, 10, 50, 250, 1,000V.
0-100, 500, 1,000V.	DC Current: 0-1, 2.5, 250 mA.
0-1000 mV.	AC Current: 0-0.001, 0.01, 0.1, 1, 10, 100, 1000, 10,000 mV.
0-100, 500, 1,000V.	Resistance: 0-10K, 100K, 1M, 2.5M ohms.
0-1000 mV.	Capacitance: 250 pF. to 0.02 uF. Inductance: 0-5,000H. Size: $5\frac{1}{2}$ x $4\frac{1}{4}$ x $1\frac{1}{2}$ inches.

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20,000 mV.	DC Volts: 0-2.5, 5, 10, 25, 50, 100, 2000, 20,000 mV.
20,000 mV.	AC Volts: 0-15, 50, 100, 500, 1,000V.
20,000 mV.	DC Current: 0-1, 2.5, 250 mA.
20,000 mV.	AC Current: 0-0.001, 0.01, 0.1, 1, 10, 100, 1000, 10,000 mV.
20,000 mV.	Resistance: 0-10K, 100K, 1M, 2.5M ohms.
20,000 mV.	Capacitance: 250 pF. to 0.02 uF. Inductance: 0-5,000H. Size: $4\frac{1}{2}$ x $3\frac{1}{4}$ x $1\frac{1}{2}$ inches.

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10, 50, 250, 1,000V.	AC Volts: 0-10, 50, 250, 1,000V.
10, 50, 250, 1,000V.	DC Current: 0-100 mA.
10, 50, 250, 1,000V.	Resistance: 0-10K, 100K, 1M, 2.5M ohms.
10, 50, 250, 1,000V.	Capacitance: 250 pF. to 0.02 uF. Inductance: 0-5,000H. Size: $3\frac{1}{2}$ x $2\frac{1}{4}$ x $1$ inch.

<b>Model C-1000</b>	<b>Price \$6.50</b>
20,000 mV.	DC Volts: 0-2.5, 10, 50, 250, 500, 5,000V.
20,000 mV.	AC Volts: 0-10, 50, 250, 1,000V.
20,000 mV.	DC Current: 0-100 mA.
20,000 mV.	Resistance: 0-10K, 100K, 1M, 2.5M ohms.
20,000 mV.	Capacitance: 250 pF. to 0.02 uF. Inductance: 0-5,000H. Size: $3\frac{1}{2}$ x $2\frac{1}{4}$ x $1$ inch.

<b>Model CT-500</b>	<b>Price \$14.85</b>
20,000 mV.	DC Volts: 0-2.5, 10, 50, 250, 500, 5,000V.
20,000 mV.	AC Volts: 0-10, 50, 250, 1,000V.
20,000 mV.	DC Current: 0-100 mA.
20,000 mV.	Resistance: 0-10K, 100K, 1M, 2.5M ohms.
20,000 mV.	Capacitance: 250 pF. to 0.02 uF. Inductance: 0-5,000H. Size: $3\frac{1}{2}$ x $2\frac{1}{4}$ x $1$ inch.

<b>Model CT-330</b>	<b>Price \$16.75</b>
20,000 mV.	DC Volts: 0-0.6, 3, 30, 120, 600, 1,2K, 3K, 6K, 10K, 15K, 20K, 30K, 50K, 100K, 200K, 300K, 500K, 1,000K, 2,000K.
20,000 mV.	AC Volts: 0-0.6, 3, 10, 20, 60, 120, 300, 600, 1,200, 2,400, 5,000, 10,000 mV.
20,000 mV.	DC Current: 0-0.001, 0.01, 0.1, 1, 10, 100, 1000, 10,000 mA.
20,000 mV.	Resistance: 0-10K, 100K, 1M, 2.5M ohms.
20,000 mV.	Capacitance: 250 pF. to 0.02 uF. Inductance: 0-5,000H. Size: $3\frac{1}{2}$ x $2\frac{1}{4}$ x $1$ inch.

## BRAND NEW SPEAKERS

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64T	8 ohms	—	—
64T	16 ohms	—	—
64T	32 ohms	—	—
64T	64 ohms	—	—
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OC44	90c	AF116	80c
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AC128	80c	BF115	80c
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OA91	20c	DA95	30c

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240 volts/3.3 Volts, 100 V.A. ... \$8.40  
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Postage 5¢

# amateur radio

JOURNAL OF THE WIRELESS INSTITUTE OF AUSTRALIA. FOUNDED 1910



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**Editor:**

K. E. PINCOTT — — — — — VK3AFJ

**Assistant Editor:**

E. C. Manfield — — — — — VK3EM

**Publications Committee:**

Ken Gillespie — — — — — VK3OK  
Harold Hepburn (Secretary) — — — — — VK3AFO  
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**Circulation—**

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**Enquiries:**

Mrs. BELLAIRS, Phone 41-3535, 478 Victoria Parade, East Melbourne, Vic., 3002. Hours: 10 a.m. to 3 p.m. only.

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★

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## CONTENTS

	Page
<b>Technical Articles:—</b>	
An Outside Broadcast Amplifier	12
Antenna Farming	14
Modern Modulation Systems	7
The Repair Bench: Doing Your Own Transistor Tests	10
<b>General:—</b>	
Cook Bi-Centenary Award	25
Correspondence	25
DX	24
Federal Comment: "One in a Million"	6
Mailing of QSL Cards	21
Meet the Other Man	23
New Call Signs	20
Overseas Magazine Review	21
Prediction Charts for November 1970	9
VHF	22
W.I.A. DX.C.C.	25
<b>Contests:—</b>	
Contest Calendar	19
Ross Hull Memorial VHF/UHF Contest, 1970-71	17
1970 Remembrance Day Contest Results: Queensland Wins	18
<b>COVER STORY</b>	
One of the most important processes in the manufacture of high precision, quality crystals, is adjusting to precise frequency by evaporation, under high vacuum. This operation is closely watched by production director, Mr. Ron Taphouse, in the Frankston, Vic., plant of Hy-Q Electronics Pty. Ltd.	

## SIDEBAND ELECTRONICS ENGINEERING

Prices are on the increase everywhere and those for Amateur equipment are no exception. However, I am proud to announce that such is still not yet the case for all lines and models advertised at the prices in my October 1970 advertisement of this magazine. On the contrary, there are two **price reductions**:

**YAESU MUSEN FT-200 TRANSCEIVER**, complete with AC power supply-speaker unit in kit form, which kit includes a \$25 extra heavy duty power transformer with 230-240-250 volt taps, especially made for me by A & R Transformers Ltd. in Box Hill, Mullard and Ducom components, a metal case of the same size and color as the FP-200 to match the transceiver, 5" speaker and explicit instructions with circuit diagram to build your own supply in one week-end and save money—the lot for only \$375. This special offer is valid only until Christmas 1970.

The second price reduction is **YAESU MUSEN FL-2000B AMPLIFIER**, with imported American CETRON 572-B valves, now only \$350.

Also: **HY-GAIN TH6DX** with balun, CDR Ham-M rotator plus 50 yards 8-cond. cable, one package \$400.

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**USED EQUIPMENT**, one of each: **YAESU MUSEN FT-200 Transceiver**, with home-brew AC supply-speaker unit .... \$300  
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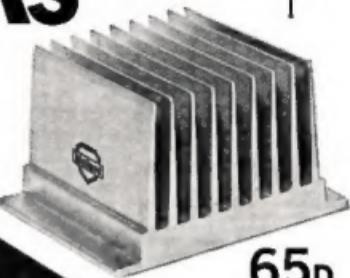
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For use with high power thyristors and silicon diodes under high peak current conditions.

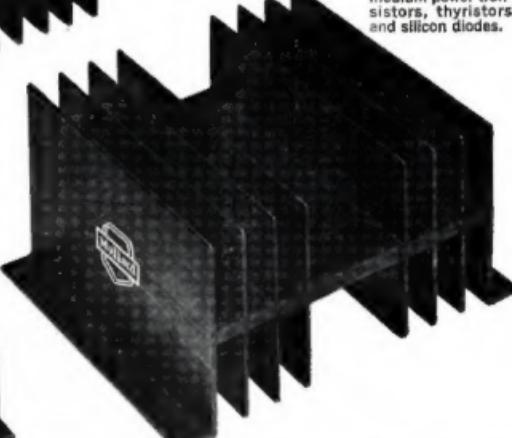
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Antenna broad-band Amplifiers, 2-30 MHz., Rotators, Co-axial Plugs, Co-axial Cable (52 or 70 ohm). Low-Pass Filters, Match Boxes. We can supply at short notice any make of antenna or accessory equipment.

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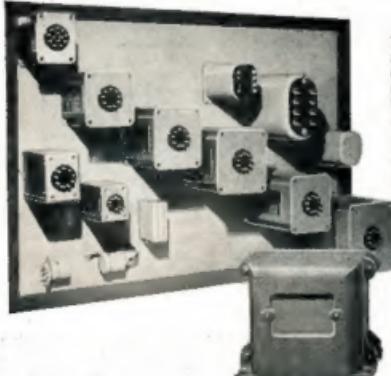
WATCH OUR FUTURE ADS FOR TOP VALUE

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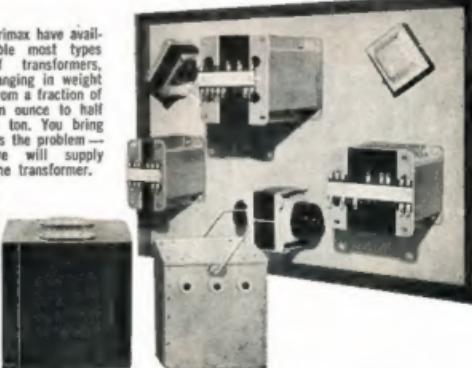
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Range 2: 8.5-18.0 MHz. Range 5: 550-1500 KHz.  
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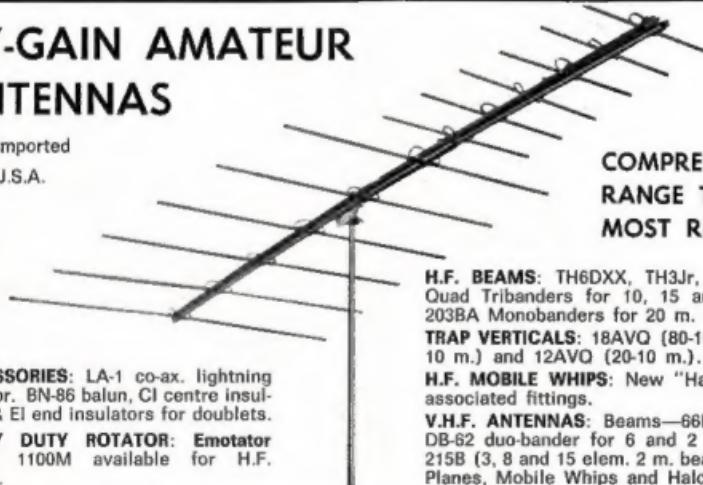
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FEDERAL

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If you are hungry, and cannot find work, or if you can and you will earn barely enough to feed yourself, and if you have never been to school—why should any hobby, let alone Amateur Radio interest you?

If you live in India and you are a Radio Amateur, you are literally "one in a million"—for in a population of 500 million people there are only some 450 licensed Amateurs.

Some of those 450 licensed Amateurs are by any standard well off. Most are not. Most are not active. They cannot compete with their equipment built with the components available to them, or with the s.s.b. stations of the rest of the world. Who works any a.m. stations on 20 metres these days? Of course components are not the only problem; I was repeatedly told while in India that hobbies are not in the blood of Indians—a hobby is an expression of a restless, seeking, Western society.

I.A.R.U. and we in our Regional organisation seek the development of Amateur Radio in countries like India. We seek to achieve this partly because we believe in what we do and we wish to share it, also partly because we believe that by contributing in some small way to the development of technology in countries like India we are doing something useful in the world around us, and partly for our own protection. It is the last point only that needs explanation.

India, to use it in the present context as an example, has, like us, one vote at International Telecommunications Union Conferences. Why should it vote to support Amateur Radio unless Amateur Radio is contributing something to its national life? The v.h.f. spectrum is a good illustration of the present development of our hobby in that country. In New Delhi I met an Amateur who is able to transmit and receive on 2 metres. There used to be two Americans and an Australian in New Delhi and together they formed a net on Sunday mornings. Now the two Americans and the Australian have left and the local Amateur awaits the appearance of someone else to talk to on 2 metres. Any frequency higher than 148 MHz. may as well not exist—in India you just cannot get the components to even try to make the equipment.

One in a million—that is the problem in India, and the problems of Amateur Radio in India are the problems of India. The two are inexorably intertwined. Is it even realistic to talk of National Amateur Radio Societies and

their international organisations rendering meaningful assistance? I do not believe that the solution lies in giving, for example, complete s.s.b. (and expensive) transceivers. This sort of charity obviously demonstrates that Amateur Radio is in fact a rich man's hobby. It teaches nothing and achieves little. The long term solution must be through the education system—such as it is. In India, education is not compulsory. This involves persuading those responsible for education that Amateur Radio as part of say, Science in clubs and schools, is a valuable tool for developing the technology of India.

Some individual Amateurs have had and have used their presence in India to assist Amateur Radio. One example is an Australian, Howard Ryder, VK3ZJY. During his stay in India as a technical specialist working with the Colombo Plan, he taught other Amateurs how to build their equipment from locally-available products. He was the Australian who started the 2 metre net I have referred to. I do not know whether he will ever realise the affection that those who he assisted have for him. Repeatedly I was asked to ask him to return, and to tell him that they need him.

Amateur Radio needs more people like Howard Ryder in places like India—people who are prepared to work amongst Indians and to know the back streets of Chandni Chowk, people who do not spend all their time in foreign lands at the bar of an intercontinental hotel.

There is room also for tangible assistance in the form of those components which are unavailable to India and which are essential to the production of equipment, such as s.s.b. transmitters.

A small boy who has never been to school and will never go to school, and who begs with head bowed while a taxi waits at a traffic light, will never be a Radio Amateur. But there are others who do attend school, who one day given the right training may become Radio Amateurs. It is these people that we must seek to influence. At the same time we lend encouragement to those who already are Amateurs to make sure that they persist with their hobby despite the difficulties that face them. Let us at the same time start at the top with those people who are capable of being Amateurs, and encourage them to become Amateurs and to encourage others to do likewise. Perhaps in our lifetime we may see in India "one in a quarter of a million".

—Michael J. Owen, VK3KI,  
Federal President.

# MODERN MODULATION SYSTEMS

R. F. DANNECKER,\* VK4ZFD

The purpose of this article is to acquaint Amateurs with modulation systems using other than sine waves and continuous signals. Pulse amplitude modulation (p.a.m.), pulse width modulation (p.w.m.), pulse position modulation (p.p.m.) and pulse code modulation (p.c.m.) are discussed, and reasons for their importance outlined.

In classical modulation systems, e.g. those represented by a.m., s.s.b., f.m., a continuous message signal is transformed into a modulated transmitted signal which is also continuous (see Fig. 1). Modern modulation systems could be called discrete communication systems. In a discrete system the continuous message signal is transformed into a **discontinuous** modulated signal. The discontinuities can be of two forms, either discontinuities in amplitude or discontinuities in time.

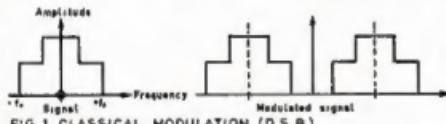


FIG. 1. CLASSICAL MODULATION (D.S.B.)  
(Note that both signals are continuous.)

The foundations for such systems were laid by C. E. Shannon working in the Bell Telephone Laboratories (about 1949). Shannon showed that if a normal (bandwidth limited to  $\pm f_0$ ) signal is sampled at (or above) a certain rate, and the sampled values transmitted; the original signal can be reconstructed exactly from the sampled signal. The importance of this result is the word **exactly**. It can be shown that the sampling must take place at a frequency equal to or greater than twice the maximum frequency in the signal ( $f_0$ ) for this to be true.

Sampling can be achieved by opening (see Fig. 2) at the required rate by a waveform consisting of a series of "spikes". Fig. 3 shows the process. Thus we obtain the simplest form of discrete communication system, namely pulse amplitude modulation (p.a.m.).

In fact the frequency spectrum of the sampled signal is a repeated version of the original signal, the amount of separation between the repeated versions depending on the sampling rate. If the sampling rate is at  $2f_0$  this is known as the Nyquist ('nigh-kwist') rate. The period between successive spikes is one nyquist interval. The effect of sampling rate on the spectrum of the sampled signal is shown in Fig. 4. In 4(b) sampling greater than the nyquist rate the repeated spectra are well separated. In 4(c) sampling at the nyquist rate the repeated spectra just touch. In 4(d) sampling at less than the nyquist rate, the repeated spectra overlap.

As stated previously, the original signal can be recovered. This is done by passing the sampled signal through a low pass filter which cuts off at frequency  $f_0$  (see Fig. 5). If the sampling were at or greater than the nyquist rate, the original signal has been recovered exactly. If the sampling were at less than the nyquist rate, the distortion introduced by overlapping of the spectra cannot be removed.

This may seem of academic interest only since p.a.m. would appear to offer

no obvious advantage over classical modulation. In practice, because of the ease with which this form of modulation may be obtained, it is often the first step in a discrete modulation system. Other forms of modulation are obtained by electronic processing of the p.a.m. wave. One such form is shown in Fig. 6(b). In this form, the pulses are of constant height, but their widths are proportional to the signal ampli-

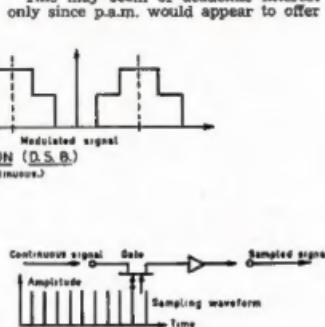


FIG. 2. SAMPLING SYSTEM.

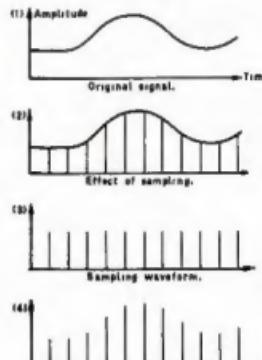


FIG. 3. SAMPLING OF CONTINUOUS SIGNAL.

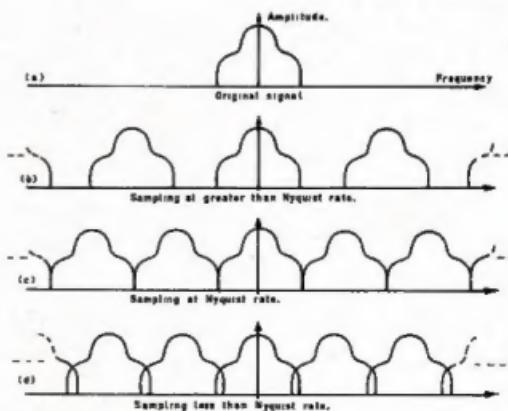


FIG. 4. EFFECT OF SAMPLING ON SPECTRUM.

\* 52 Pohman Street, Southport, Qld., 4215.

tudes at the sampling times. This form may be obtained from pulse amplitude modulation by passing through an amplitude to time converter. This second form of discontinuous modulated signal is known as pulse width modulation (p.w.m.).

If a p.w.m. wave were differentiated, the form shown in Fig. 6(c) would be obtained. The positive going pulse at the leading edge of each pulse contains no information and so could be removed, leaving the negative going pulses shown inverted in Fig. 6(d). In this form of modulation it is the position of the pulse which ultimately reflects the amplitude of the originating signal. This form is called pulse position modulation (p.p.m.).



FIG. 5. EFFECT OF LOW PASS FILTERING ON FIG. 4.

A fifth form of discrete modulation which requires more consideration than the previous types is obtained if we take each pulse height in a p.a.m. wave and convert this amplitude into a binary number representing the height.

The binary numbering system involves powers of 2 while the common system involves powers of 10, e.g. one hundred and sixty-five in the decimal system would be represented as:

$$\begin{aligned} 1 \times 10^4 + 6 \times 10^3 + 5 \times 10^2 \\ = 1 \times 100 + 6 \times 10 + 5 \times 1 \\ = 100 + 60 + 5 \\ = 165 \end{aligned}$$

in the binary system this would be represented as:

$$\begin{aligned} 1 \times 2^7 + 0 \times 2^6 + 1 \times 2^5 + 0 \times 2^4 + 0 \times 2^3 + 1 \times 2^2 + 0 \times 2^1 + 1 \times 2^0 \\ = 1 \times 128 + 0 \times 64 + 1 \times 32 + 0 \times 16 + 0 \times 8 + 1 \times 4 + 0 \times 2 + 1 \times 1 \\ [= 128 + 0 + 32 + 0 + 0 + 4 + 0 + 1] \\ = 1 \quad 0 \quad 1 \quad 0 \quad 1 \end{aligned}$$

The advantage of the binary system from an electrical viewpoint is that a sequence of ON or OFF states rather than by a sequence of 10 discrete levels as would be required for a decimal representation.]

Thus a pulse of height 13 volts might be represented by the number 01101 and a pulse of height 20 volts by the number 10100. A different form of modulation would then be obtained if instead of sending a single pulse in each nyquist interval, a sequence of say five pulses were to be sent during that time with each pulse being either one or a zero, so as to form the binary number representing the original sampled height in that nyquist interval. In this form the sample heights have been encoded into binary numbers and the form is referred to as pulse code modulation (p.c.m.).

It is necessary to limit the number of pulses in the sequence due to practical considerations. If we allow five pulses in each nyquist interval to repre-

sent the amplitude of the pulse, then the maximum number of possible different levels which can be distinguished will be  $2^5$  (= 32). Suppose the maximum voltage in the signal is say 32 volts; suppose also the amplitude of the actual signal at successive sampling times is as shown. Then the binary number (given in decimal form) closest to each amplitude will also be as shown in Table 1.

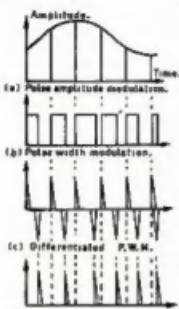


FIG. 6.

In fact the net effect of this finite number of quantisation levels is the same as if noise were added to the original signal. By analogy with this case, the error is referred to as the quantisation noise. Quantisation noise is an additive noise, similar to naturally occurring noise due to atmospheric, etc., in standard communications systems. However, just as the addition of

It can be shown that the capacity of a communications system is given by:

$$C = W \log_2 (1 + SNR)$$

where  $C$  = capacity of system

$$W = \text{bandwidth}$$

$$SNR = \frac{\text{signal power}}{\text{noise power}}$$

It is clearly seen that given the value of signal-to-noise ratio and bandwidth  $W$ , the capacity  $C$  of the system is determined. Should this capacity not be sufficient for some particular purpose (e.g. high speed data), then either the SNR must be increased by increasing the signal power which is transmitted, which may not be possible, or  $W$  must be increased. Increase of bandwidth  $W$  is sometimes the only means of increasing system capacity (e.g. spacecraft). There are a variety of ways used to increase  $W$ . (In classical modulation f.m. occupies more bandwidth than a.m.) In particular, conversion of the signal into any of the pulse modulated forms which we have considered will result in an increase, so that for a given noise level, the fidelity (readability) of systems employing this method is inherently better than would be obtained if the original signal were say amplitude modulated. This is one reason for the increasing modern use of these methods.

In practice the encoding of p.c.m. can be modified in a number of ways.

To properly decode a p.c.m. sequence (word), the receiver must know the position of the start of each word, or it may decode bits from two adjacent words. To overcome this, a few bits are added at the start of each word, which have a fixed waveform and can be easily recognised. These bits comprise the "sync code," and provide word synchronisation. The total number of bits per nyquist interval must then be greater than the number required to give the amplitude of the signal at that time. The complete sequence, sync bits plus information bits, is called a "frame". (See Fig. 7.)

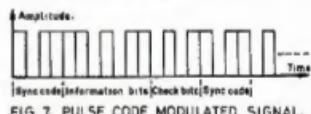


FIG. 7. PULSE CODE MODULATED SIGNAL.

natural noise prevents the exact recovery of a signal, so the addition of quantisation noise also prevents an exact representation of the original message being obtained. Quite obviously the quantisation noise can be reduced by increasing the number of pulses in each sequence. This means that an improved signal will then occupy more bandwidth than previously.

Nyquist Interval	t0	t1	t2	t3	t4	t5	t6	t7
Actual Amplitude	20.0	19.1	16.5	12.8	3.2	7.7	14.9	8.4
Sample Amplitude	20	19	17	13	3	8	15	6
Error	0	-0.1	+0.5	+0.2	-0.2	+0.3	+0.1	-0.4

Table 1.

ity check bits. These check bits are calculated on the information bits, e.g. parity check bits are set at 0 if the checked information bits contain an even number of ones and are set to 1 if the information bits have an odd number of ones. If information bits are then altered during transmission, the even-odd correspondence with parity check digits will be altered. This should be detectable by comparing parity checks with information bits, and the bits in error can be corrected. A code containing parity check bits in this way is an "error correcting code".

A further advantage arises in the use of a binary coding system in that the receiver has only to decide if an incoming signal is a 1 or a 0 rather than some particular level out of a large number of possible levels. The detector can be a simple level detector to give zero output if the incoming signal is below a certain level corresponding to a 0 and

to give an output if the incoming signal is above this level corresponding to a 1. Obviously such a system can be made very accurate even for low SNR and the process can be improved further by the use of optimum or Wiener filtering in the system.

In conclusion it should be pointed out that a practical p.c.m. system is quite complex and, at least for the present, is beyond the financial reach of most Amateurs. Much research is being carried out into p.c.m. and in the future its use will become increasingly widespread.

I should like to acknowledge the valuable assistance given in the preparation of this article by Dr. L. V. Skatertbol of the Department of Electrical Engineering, University of Queensland.

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## PROVISIONAL SUNSPOT NUMBERS

JULY 1970

Dependent on observations at Zurich Observatory and its stations in Locarno and Arona

Day	R	Day	R
1	137	16	61
2	155	17	59
3	155	18	56
4	159	19	52
5	163	20	52
6	161	21	188
7	152	22	115
8	113	23	106
9	104	24	116
10	98	25	122
11	81	26	138
12	76	27	145
13	79	28	146
14	68	29	135
15	61	30	122

Mean equals 115.5

Smoothed Mean for January 1970: 106.2

Predictions of the Smoothed Monthly

Sunspot Numbers

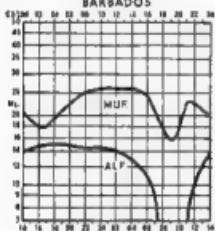
August	September	October	November	December	January
85	83	81	88	87	85

—Swiss Federal Observatory, Zurich

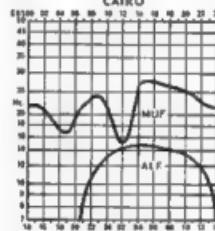
## PREDICTION CHARTS FOR NOVEMBER 1970

(Prediction Charts by courtesy of Ionospheric Prediction Service)

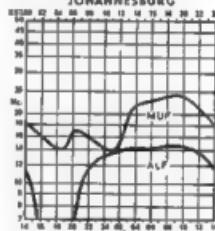
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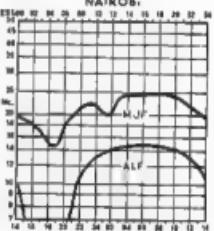
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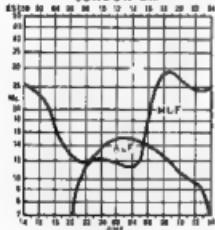
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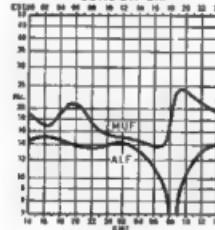
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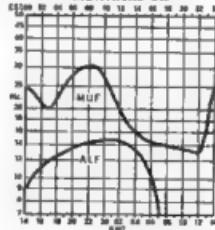
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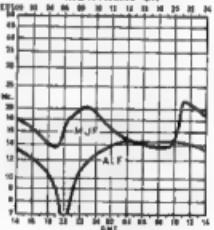
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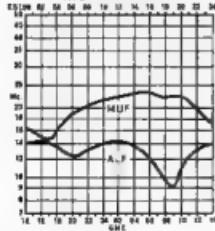
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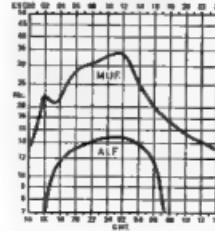
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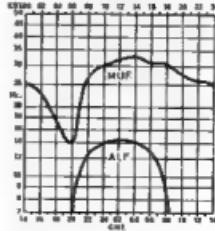
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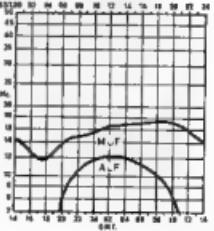
### SAN FRANCISCO



### TOKYO



### WILKES



## Doing Your Own Transistor Tests

LARRY ALLEN

To hear some guys talk, it, a transistor is the easiest thing in the world to test. But others don't agree. A transistor to them is still a mystery.

Well, the truth is, most transistors can be tested without complicated equipment, gimmicks, calculations, or formulas. To keep it simple, there are just two basic things you need to find out about a transistor: (1) Does it work at all? (2) How well?

## TRANSISTOR PARAMETERS

That word "parameters" scares off a lot of Hams. It conjures up complicated graphs with bent lines and long formulas with Greek symbols and big and little letters. All the word actually refers to is conditions of operation.

One transistor manual lists 103 possible parameters. They're great for a transistor designer. But a lot fewer is plenty for testing on the repair bench. In fact, I won't even use the term "parameters". Instead, I'll just tell you about the voltages, currents and resistances that tell you how a transistor is doing.

I'll start with the diagram of a simple transistor stage in Fig. 1. This is a grounded-emitter amplifier—probably the most common transistor stage in use today.

The transistor is NPN. Bias is forward when the base is slightly positive with respect to emitter. The collector is "far" positive with respect to emitter.

A PNP transistor takes negative voltage on the base to forward bias the emitter-base junction. That's not necessarily a negative voltage to ground, but to emitter. The collector of a PNP operates "far" negative from the emitter.

## WHICH WAY IS UP?

Some Hams I've talked to about transistors seem confused by operating voltages. One key to understanding is knowing how to describe the voltages.

For example, in Fig. 1, if the base voltage changes to 0.1 volt, it has obviously become less positive. That means less positive with respect to wherever you're measuring from, and for most measurements that is ground.

Look at the same voltage with respect to the emitter. As it's labeled on the diagram, the base is normally more

positive than the emitter by about 0.3 volt. (The emitter is 0.15 volt, and the base is 0.45 volt; between the two is 0.3 volt, the base more positive than the emitter.)

Know what that means? "More negative" is exactly the same thing as "less positive". And "more positive" means the same as "less negative".

If the base voltage in Fig. 1 drops to 0.1 volt, the voltage relationship between base and emitter changes. The difference is then 0.05 volt (0.15 minus 0.1 equals 0.05), but the base has become less positive than the emitter. That's the same as saying it is more negative than the emitter. The emitter-to-base bias has become 0.05 volt negative. (Call it emitter-base bias, not base-emitter bias. You want the emitter as the point of reference, so name it first.) An NPN transistor with the base negative is reverse-biased. Collector current can't flow.

This should make clear that, even though you measure voltages with your voltmeter common lead connected to ground, the important thing is the voltage between elements of the transistor. In most transistor stages, your chief interest is the voltage between emitter and base; of secondary interest is the voltage between emitter and collector.

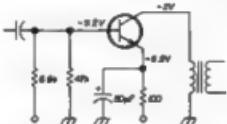


Fig. 1—Common base transistor amplifier is popular in Amateur equipment.

Suppose someone tells you the base voltage on one of these transistors has gone "up". What does that really mean? Usually he means the voltage is higher in the polarity shown on the schematic.

Consider the base voltage in Fig. 2. It appears "lower" than the emitter voltage. Its value is less. Measured to ground, the base voltage is less negative than the emitter voltage. The important thing is this: being less negative, the base is more positive than the emitter. That provides forward bias for any NPN transistor.

If the base voltage goes up—that is, if it goes further negative with respect to ground, as the voltmeter measures—the bias actually decreases. Say the meter measures -0.4 volts. The base has become more negative than it was. Looking from the standpoint of emitter-base bias, it tells you more if you say bias has become less positive. Forward bias is therefore reduced. Your voltmeter thus shows base voltage higher than before, but bias is less.

These are important relationships in transistor repair work. The simplest way to combat this seeming ambiguity is to quit using such vague notions as "up" and "down" for voltage measurements. Form the habit of thinking more negative or less positive, more positive or less positive.

## TESTS THAT REVEAL

At the repair bench you are usually concerned with a transistor in some piece of equipment. Tests you can make without unsoldering the transistor are the handiest.

There are three ways to evaluate a transistor in that circumstance. Two additional tests can be made if you unsoldered one or two transistor connections.

Finally, two quick test procedures evaluate a transistor outside the circuit. They are especially handy if you have a batch of unidentified transistors you want to check out. Even these tests can tell you more about transistor quality than you might expect.

## VOLTAGE MEASUREMENTS

Once you examine d.c. flow in transistor stages, you can figure out a lot from the voltages. If a voltage is wrong, deduction can tell you whether it's the transistor or something external.

Pretend the stage in Fig. 3 is giving you trouble. Your voltmeter tells you the base actually has -0.5 volts on it instead of the low -0.45 volt that's normal. Think out the possible causes.

Could be one of the base resistors is bad. But collector-base leakage in the transistor is far more likely. You can verify by disconnecting the base lead of the transistor. If voltage on the open base lead is still highly negative, the transistor junction is leaky.

Or, in the same stage, suppose the emitter measures -0.9 volt. For some reason, more current than normal is flowing in the 52-ohm resistor. The emitter voltage is measured across. The transistor is probably drawing too much current.

But is that due to overbias or a transistor defect? If base voltage remained about the same, the trouble is likely in the transistor. You see, -0.9 volt at the emitter, with only -0.45 volt at the base, constitutes reverse emitter-base bias for this PNP transis-

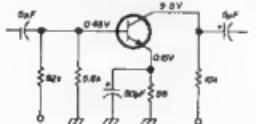


Fig. 2—Common base PNP transistor amplifier works the same as NPN, only change involves voltage polarities on the various elements.

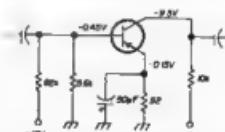


Fig. 3—PNP transistor in the common base stage works the same as NPN, only change involves voltage polarities on the various elements.

sistor. That would reduce current through the transistor, not increase it unless the transistor happens to be defective.

There are plenty of other examples of this kind of reasoning. Just remember which polarity of transistor you're dealing with and the likely effects of voltage changes. And don't forget to interpret voltage measurements in terms of their relation to each other and to the transistor itself.

The other two in-stage test ideas utilize a transistor's bias characteristic. For most transistors, zero and reverse bias cause zero collector current. A healthy forward bias assures significant collector current. These precepts of course apply only if the transistor is not defective.

The first test is for stages in which the transistor operates with forward bias. You can determine that from the schematic. Remember, forward bias is base-positive for an NPN transistor and base-negative for a PNP.

Connect your voltmeter at one of the points shown in Fig. 4. Several possible connections are illustrated. If you need it, you can insert the 100-ohm resistor;

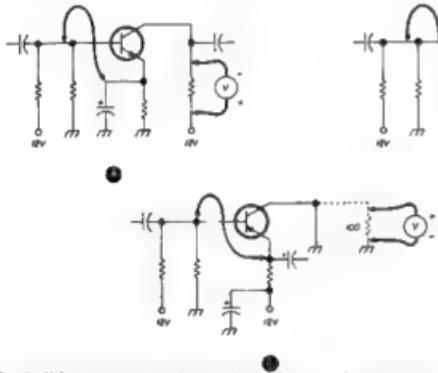


Fig. 4—Voltmeter connections in several amplifier stages for making bias-change operation tests. Idea is to eliminate bias on stages that normally use forward bias and add it to those that don't, while watching the change in collector current. You can add a resistor if the collector circuit doesn't have one.

its value won't bother the circuit much. Indirectly you are measuring collector current.

Notice the voltmeter reading. Then clip a shorting jumper between base and emitter. The voltmeter reading should drop to almost nothing. If it doesn't, the base isn't controlling collector current.

The second test is for stages where zero or reverse bias is normal. (The transistor may conduct, but probably during only a small portion of each signal cycle, leaving an average or d.c. bias that is zero or reverse.) The voltmeter connections are the same as in Fig. 4.

This time, instead of eliminating bias by shorting base to emitter, you apply a definite forward bias to base. Figure out from the schematic what would constitute forward bias for the transistor. Then somehow alter the bias to make it temporarily forward. The meter reading should take a definite move upward, signifying more collector current.

For instance, the NPN transistor in Fig. 4A has forward bias only when the base is more positive than the emitter. How do you make it more positive? One way is to reduce the value of the supply resistor, since it goes to a positive voltage source. Just bridge it with a low-enough resistance to make the base more positive than the emitter. If the transistor is working normally, the voltmeter shows more collector current.

In Fig. 4B the basic supply scheme is different. But the transistor is still NPN. Forward bias requires base to be more positive than emitter, same as always. But how can you make it that way? Just remember that more positive is the same as less negative. Bridge a lower resistance from base to ground, low enough to reduce the base voltage to a value less than at the emitter. Collector current goes up. If not, the transistor isn't responding as it should.

The transistor in Fig. 4C is PNP. Forward bias demands a base more negative (less positive) than the emitter. It should be now be easy for you to figure how to make this base less positive. When you do, the voltmeter should register higher collector current.

there should be almost non-existent. Unwanted leakage lets current across the junction to the meter.

## TESTING OUT-OF-CIRCUIT

If you have a transistor tester, fine. With a good one you can test transistors in or out of the stage faster than with the tests I've outlined here. But if you don't have one, you may often need these procedures.

Tests outside the stage are popular with Hams. The basic instrument is your ohmmeter. There are two main purposes. One is identification. The other is evaluation.

Hams often pick up transistor "bargains". You met a handful of odd-lot transistors, often unmarked or marked in some way that means nothing to you. You may not even know which wires go to emitter, base, or collector. Here's how to settle these doubts.

An ohmmeter with 1.5 volts or less between the test leads is safest (measure with some other voltmeter). More voltage might pop a transistor junction. Also, notice which test lead has the positive voltage and which the negative; you'll need to know for these tests. Nowadays, it seems most ohmmeter batteries are connected with positive voltage on the common or black test lead.

Pick any two transistor wires. Clip the ohmmeter to them in first one direction and then the other. If you get no reading, try another pair, again measuring in both directions.

When you get a low ohms reading (150 or less), one of the ohmmeter leads is clipped to the base wire. The way most transistors are arranged, it is the wire in the middle.

But you can make sure. Leave one ohmmeter lead clipped to the wire you think goes to the base. Move the other lead to the remaining transistor wire. If the ohmmeter reading is again low, the lead you didn't move is definitely clipped to the base. If not, the one you moved was.

You can now identify the transistor type. When you get low readings to both other elements with the positive ohmmeter lead connected to the base, you are testing an NPN transistor. A PNP transistor gives low readings when the negative ohmmeter lead is clipped to the base.

You've identified the base, but you don't know which of the other two wires goes to the collector. There were clues in years past, but you can't trust the dots, stripes, and tabs on today's myriad of transistors. And basing diagrams aren't standard enough to help much either.

Start with the ohmmeter connected to show low resistance between the base and either of the other elements. You know which wire is base, so unclip that lead and move it to the other unidentified wire. The meter should read infinity, or open. If not, the transistor is defective.

Then click the range switch of your ohmmeter to higher scales until you see a slight downward meter deflection (something less than infinity). This usually happens on the Rx10K or Rx100K range. Next, reverse the two ohmmeter leads. The ohms reading will

(continued on page 16)

# An Outside Broadcast Amplifier

## LECTURE NO. 9

C. A. CULLINAN,\* VK3AXU

The original 3CS O.B. Amplifier No. 4 was manufactured in 1960 and after considerable work it could no longer meet the Australian Control Board's standards.

It was decided, therefore, that as part of our training programme that this amplifier would be dismantled and a new one built to take its place, the work to be done by our Cadet and to correspond with the appropriate part of the Marconi School course. The new amplifier would use as many components as possible from the old amplifier but would be different in mechanical construction and somewhat different in circuitry to avoid making a direct copy, as it was felt that little was to be gained in tuition in making a copy.

### DESIGN AND NOTES

A single channel Outside Broadcast Amplifier to be built using valves and operated from the a.c. mains.

The amplifier must meet the Australian Broadcasting Control Board standards, and, where applicable, Australian Post Office specifications.

The only suitable output transformer, which was available, was an A. & R. type OT2629 for which a manufacturer's test certificate was held (22/4/69), in respect of A.P.O. Specifications 1033 and 1084.

Details of this transformer are:

Primary Impedance: 7,000 or 5,000 ohms, single ended.

Secondary Impedance: 500, 250 or 125 ohms.

Power Rating: 5 watts.

Frequency Response: 50 Hz. to 30

KHz.  $\pm$  2 dB.

### Output Valve

The output transformer is suitable for use with any valve requiring a plate load of 5,000 or 7,000 ohms, and taking a plate current of 50 mA. Thus the choice falls mainly between types EL84/6BQ5, 6MS, 6GW8 or 6V6GT. As a large number of EL84s are used in studio equipment, this type was chosen as the output valve, with 160 ohm cathode bias resistor. A simple resistor of this value was not available so some calculations were made to determine which of two 3 watt w.w. resistors on hand would give the necessary value when used in parallel. The two resistors were 250 ohms and 450 ohms, which in parallel become 160.7 ohms.

### Other Valves

In order to meet the specified noise figures it is essential that the other valves must be of very low noise type and for this reason EF86 valves were selected. This type was first available in Australia somewhere in late 1954 to 1955. It is also known as 6BK8/2729, and was specifically designed for use in low level microphone or pick-up pre-amplifiers. It uses a 9-pin minia-

● Continuing the series of lectures by C. A. Cullinan, VK3AXU, at Broadcast Station 3CS for students studying for a P.M.G. Radio Operator's Certificate.

ture base, has internal shields and a specially constructed heater-cathode system.

It is possible with proper design of equipment to reduce hum and noise voltages, referred to the control grid, to the order of 1.5  $\mu$ V. for hum and 2  $\mu$ V. for valve noise for an audio frequency bandwidth of 15 KHz.

In recent years an improved EF86 has made its appearance. For this valve, the previous mesh type anode (plate) has been replaced with a solid one. This gives additional shielding and reduces pick-up of external magnetic fields (hum) by as much as 6 dB. It would appear that the EF86 is a later development of the valve type EF40.

For many years the designer has used EF86 valves as pentode audio frequency amplifiers with a plate load of 0.22 megohm, a screen resistor of 1 megohm, and a cathode resistor between 2,200 ohms and 3,000 ohms. With a cathode current not in excess of 1 mA. and cathode bias not less than 1.6 volts, excellent gain, low distortion and low noise have been achieved for a bandwidth of 15 KHz.

If they are available, the student is referred to the following publications for further details of the EF86/6BK8/2729 valve:

Radiotronics, Vol. 20, No. 6, June 1955

Radiotronics, Vol. 22, No. 5, May 1957.

Mullard Circuits for Audio Amplifiers.

Philips Valve Data Handbook.

Calculations showed that with a microphone transformer having a turns ratio of 1:44.7 and a 6 dB attenuator between the output transformer secondary and the amplifier output terminals, the specified gain of 80 dB. could be obtained by using two resistance coupled EF86 valves and an EL84 output valve, whilst applying considerable feedback over the last two stages.

Thus the amplifier portion of the design resolved itself into a three-stage amplifier, using EF86s in the first two stages with an EL84 in the output stage. Negative feedback to be used from the plate of the output valve to the cathode of the second valve.

Because the specifications state that the output of the amplifier is to be balanced and floating, it is not possible to use negative feedback from the secondary of the transformer. Also, the particular output transformer does not have a tertiary winding for feedback

purposes, therefore the feedback was taken from the plate (anode) of the output valve.

The input transformer is of the specifically shielded type made for low level applications. The heavy shielding reduces hum pick-up as much as 40 dB. below that picked up by a similar, but unshielded transformer.

The gain control is located, electrically, between the first and second stages.

### POWER SUPPLY

The specifications stipulate that silicon diodes are to be used as rectifiers in the power supply.

S.T.C. EM410 silicon diodes were used as they were in our stock of spare parts. These diodes have the following characteristics as abstracted from an S.T.C. I.T.T. Application Note:

Peak inverse voltage (p.i.v.), 1,000 volts.

Average rectified current at 85°C., 0.5 amp.

Operating and storage temperature range,  $-55^{\circ}\text{C}$ . to  $+135^{\circ}\text{C}$ .

Voltage drop approx., 1.2 volts.

Consideration was given to the use of an Itroncore T5/102 power transformer which was available and was suitable. The following information was extracted from the maker's data sheet:

H.t. secondary voltage, 225-0-225, i.e. 225 volts each side of the centre tap.

H.t. secondary current, 50 mA.

Heaters, 6.3 volts at 2 amp.

An astatic shield is fitted between primary and secondaries to reduce capacitive coupling between these windings. In addition, it has an external eddy-current shield.

As the h.t. secondary has a centre tap, this means that a full wave rectifier circuit must be used.

Having selected the power transformer and the type of silicon diodes, it becomes necessary to determine how many diodes will be needed.

The term peak inverse voltage means the peak voltage that the rectifier can withstand in the reverse direction before it breaks down. This voltage includes both a.c. voltage and the d.c. output voltage.

Other terms used in place of peak inverse voltage are crest working reverse voltage (v.r.w.m.) and peak reverse voltage (p.r.v.). They all mean the same thing.

Now one of the characteristics of silicon diodes is that they are very liable to break down the moment the p.i.v. is exceeded. Some will be destroyed instantly, but others will recover if the excess is not too great.

Again from S.T.C.-I.T.T. Application Note, we take the information to enable us to determine the various voltages to be expected.

P.i.v. =  $3.14 \times$  volts out

V.r.m.s. =  $1.11 \times$  volts out.

Volts out = volts r.m.s.  $\pm$  1.11.

Volts r.m.s is the r.m.s voltage from the h.t. centre tap to either high voltage end of the h.t. secondary winding

Now let us do some calculations.

The a.c. r.m.s voltage across one half of the h.t. secondary is 225 volts. Therefore the d.c. output voltage will be:

$$225 \div 1.11 = 202.7 \text{ volts}$$

and the p.i.v. will be:

$$202.7 \times 3.14$$

However, this is for a choke input filter, but when a large condenser is connected across the output of the filter and the power supply is switched on, the output voltage will be much higher until the filter input condenser becomes fully charged and the valves have warmed up.

At the instant of "switch on" there is practically no load on the power supply so the output voltage of the rectifier system soars considerably.

In this amplifier the measured d.c. output from the rectifier at "switch on" was 340 volts.

For safety, it is necessary to take this new voltage as the d.c. output voltage (when the amplifier is warmed up this voltage will drop to 250V).

Therefore the p.i.v. will be:

$$340 \times 3.14$$

$$= 1,067.6 \text{ volts.}$$

To allow for variations in a.c. mains voltages, also switching transients that may show up in the a.c. mains, it is desirable to add at least 25% to this value, i.e.  $1,067.6 + 266.9 = 1,334.5$  volts.

The simplest way to accommodate this voltage is to put two diodes in series in each leg of the transformer. We selected EM410 diodes as they are rated at 1,000 p.i.v.

When a large condenser is used at the input of the power supply filter it is necessary to protect the diodes from burning out due to excess current through them as the rectifiers start to charge the condenser.

To avoid this problem, it is necessary to use a transformer having sufficient impedance to restrict this current flow or to put resistance in series with each h.t. leg of the transformer.

In this design, the 80  $\mu$ F. condenser is not excessively large and the impedance of the power transformer keeps the current within the limits of the diodes.

One problem of putting diodes in series is that sometimes they will not share the voltage between them, therefore a 1 megohm 1 watt resistor is wired across each diode.

#### PRACTICAL NOTES

The lead from the microphone transformer to the grid of the first EF86 was made as short as possible and shielded with braid fitted loosely to reduce the capacity between the lead and the braid.

A piece of 1" o.d. co-axial cable was used as the lead between the 0.022  $\mu$ F. coupling condenser and the top of the gain control, which was about 4" above the top of the chassis. The braid was earthed as close to the 0.022  $\mu$ F. con-

denser as practicable. The other end of the braid was connected to the "earthy" end of the gain control. Any gain control was not earthed in any other manner.

The lead from the arm of the volume control to the grid of the second valve was also a piece of co-axial cable, with its braid earthed as close to the grid as possible. At its other end the braid was insulated so that it could not touch anything.

All these precautions were taken to reduce, as far as possible, frequency loss at the higher frequencies.

As part of tuition, the co-axial cable was replaced with tightly woven shielded wire. The frequency response at 10 KHz. immediately dropped to 5 dB. below that of 1 KHz.

**Heater leads:** The heater leads between the EF86s and the EL84 were twisted and shielded, also care was taken in the layout so that no heater lead passed near a grid pin in a valve socket.

**Headphone Jack:** This was insulated from the chassis to maintain a floating output as specified. Two 500 ohm resistors prevent a short circuit across the amplifier output should the headphones plug not be properly inserted.

**Layout:** An aluminium chassis was used to reduce hum transfer from the power transformer to the input transformer, as could happen with a steel chassis.

The power transformer was mounted in a rear corner of the chassis. The location of the output transformer was determined as follows:

After carefully insulating leads, a.c. power was fed to the power transformer to energise it.

Then a 7,000 ohm resistor was wired to the 7,000 primary of the output transformer and the 500 ohms secondary was connected to the A.W.A. Noise and Distortion Meter.

The 50 Hz. (hum) pick-up from the power transformer was measured with the N. & D. meter, after which the transformer was moved over the surface of the chassis to locate the position of minimum hum.

The location of the microphone input transformer was determined in a similar manner, using the high impedance input to the N. & D. meter connected to the transformer secondary, the primary being terminated with a 47 ohms 1 watt resistor.

Locating the transformers in this manner proved to be most successful as no hum can be detected in the completed amplifier.

The amplifier was fitted into a metal case, with carrying handles.

It is a matter of great satisfaction that the completed amplifier meets all the designed specifications and is a welcome addition to the station's O.B. equipment.

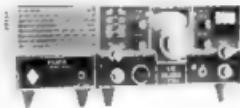
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#### SOLDERING IRONS

A range of corrosion resistive soldering irons in a variety of bit sizes and wattages for radio work is now available. Manufactured by Birko Electric Pty. Ltd., these soldering tools have a stainless steel casing, and are fitted with a no-heat transfer moulded handle. Power ratings for the 230V. a.c. types ranges from 40 watts to 80 watts in the radio work purpose models, and 130 watts to 200 watts for the general and workshop heavy duty models. An instant heat model, with a finger touch heat control, operates from 8 to 6 volts d.c. or a.c. (through step-down transformer) will be found ideal for Amateur work.

A technical brochure is available on all models from Birko Electric Pty. Ltd., 26 Victoria Crescent, Abbotsford, Vic., or from electrical and radio wholesalers.

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# ANTENNA FARMING

A. J. C. THOMPSON,\* VK4AT

A 10 element long type Yagi on 7 MHz.—a.m. at s.s.b. strength.

The reaction to the above circumstances have followed a fairly set pattern. Some were expected, some should have been expected, some were quite unexpected. From the reports received, the following are fairly representative:

- (1) The fact that it is a.m.
- (2) The unexpected strength.
- (3) The good quality of the transmission (where the gear was capable of judging it).
- (4) The way it bashed down the QRM.
- (5) Its good effect on QSB.
- (6) Its effect on the background noise level.

In addition to the above, the most interest was taken in:

- (1) The number of elements used on 7 MHz. (10 or 13).
- (2) The low height (20 feet poles).
- (3) The use of steel wire.
- (4) The valley QTH.
- (5) Why such a scheme was attempted.

I will try and get things straight right here. This article cuts no new ground scientifically. It does deal with some theories, but only the practical application of them, that would not be found in text books or come to the notice of Radio Amateurs under normal circumstances. I am not an expert on any subject because I write about them, or because I can make such a row in the Southern States on 7 MHz. at night time. All these things came about because my QTH is in a very short valley completely surrounded by hills. 120 foot towers fail to bring in the t.v. channels from Brisbane, 100 miles distant. 7 MHz. is equally unco-operative, but 3.5 and 14 MHz. (also some other bands) appear to be much better.

It is evident then that sheer necessity is the driving force behind the construction of this antenna farm. Being an antenna farm, ease of construction is a must. Such construction means light-weight gear just as it does in industry. It also means low costs. Probable gain must be in proportion to both the work involved and the costs. This is a ratio—work and costs against gain. It sets the pattern at all times. An application of this ratio to the long type of Yagi will dampen a lot of enthusiasm. It means much work—low costs—much gain and in addition an area or boom length in proportion (half an acre for 7 MHz. [0.8 acre for 13 elements], quarter of that for 14, etc.) Interested persons will now only be.

- (1) Those with adequate areas,
- (2) Scouts Clubs, etc., with more enthusiasm than cash,
- (3) V.h.f. where boom lengths cause no dismay.

Such a beam was constructed on Channel 4, necessity being the driving force on that occasion also. For the

benefit of those with little interest in Yagis, a little explanation is necessary. Maximum gain necessitates very critical tuning of the beam. This in turn means the use of gear beyond our reach. The same results can be obtained from book-values (with much less critical dimensions) by the use of more elements. For example, I spent months tuning up a 5 element Yagi and then found that I had the same spacing as those given in a text book.

For a practical explanation on the use of Yagis, I will take the position right here. Such a beam with 5 elements was already working quite well on 7 MHz. and I desired more gain. More elements meant two posts and two poles for each additional element. If I added an element at 0.1 wavelength spacing, the gain was small and in addition it could easily upset the impedance, and so be less. In the alternative method, that of re-constructing the whole antenna at 0.35 wavelength spacing, the work-cost-gain ratio was also unfavourable. Either the gain had to increase or the work decrease. Such an unlikely event actually did occur with the published reports of this combined type of Yagi. In it (now called the Long Type Yagi) the high gain of the original Yagi was retained in the front end of five elements and, without upsetting the impedance values, the additional elements at 0.4 wavelength spacing were added. Two things made this possible:

- (1) It was ascertained that it was not the number of directors used that gave the gain, but the boom length that they occupied, provided that the ratio space-length-diameter of el. was adhered to.
- (2) At that distance and spacing, the additional elements did not upset the impedance of the driven element.

These circumstances made the ratio work-cost-gain very attractive. Construction on both 7 MHz. and Channel 4 were commenced. An additional characteristic was the fact that the back-to-front ratio increased with closer spaced elements, but wider spaced elements of this magnitude gave good signal side rejection. This latter characteristic looked good as an image rejector on Channel 4. Our very local t.v. translator put beautiful images on our sets corresponding to a mountain rock face plus five timbered high spots on the ridge opposite. With the aid of an iron roof, suitably positioned, and this type of Yagi very good pictures resulted.

The antenna took only a couple of hours to construct. It was made from the plastic covered type of conduit (10 cents a foot) with No. 10 fencing wire inserted and soldered. This gave a very firm connection, and the elements could be bent at any angle. Joints of the conduit are easy with a 6 in. saw cut and a slarter of another inch. This shows that quick, easily constructed beams for v.h.f. are possible for casual experi-

ments. Conduit is available in various lengths and diameters. The sag involved on the longer lengths are easily braced.

Now to return to the set-up here on 7 MHz. Steel wire of 14 or 16 gauge was used of the type used on fruit cases. The weight and strength was far beyond what was necessary, but it was available on this farm. Fence posts and poles were also available, but were also much heavier than was necessary. The insulators used were very light and efficient, being  $\frac{1}{2}$  to 1 inch cut off 1 inch diameter water pipe of the polystyrene type. Higher grades may be better, but some are weather affected. Much relevant material will be found in a previous article ("A.R.", March 1970). Because of the scaling factor, experiments can be changed from one band to another, although "doubling up" too much runs foul of the fact that you are not scaling up the surroundings too.

In the previous article it was shown that on 14 MHz. the forward gain dropped sharply when the antenna was lowered from quarter to eighth wavelength height. This deduction was based on the fact that W land, on which it was aimed, decreased in strength, while the JAs came up. A perusal of many text books gave little information on this problem. Most of them stop at half, but a few go to quarter wavelength height. By continuing a graph, it was assumed that the difference in the angle of radiation would be in the vicinity of 8-10° for one-eighth and one-quarter wavelength heights. Against this assumption was the extraordinary behaviour of antennas at:

- (1) Ground level,
- (2) A few inches underground,
- (3) Inside metal pipes, both open and closed,
- (4) Wire in water.

If you want a headache just read about those things. One significant fact emerged. At zero height, much gain was lost, but the signal-to-noise ratio was more favourable. If then, the gain lost by reducing the wavelength height down to one-eighth could be recovered by adding more elements, then the signal would come up more than the QRM. On such a band as 7 MHz., this matter is of major importance.

From my own experience, further experiments seemed to be futile, but a 5 element Yagi at one-eighth wavelength height on 7 MHz. had actually shown some gain. It was decided to change the experiments from 14 to 7 MHz. and accept the loss due to the lower height, because the use of 20 ft. poles made the scheme a practical proposition. As previously mentioned, the adverse ratio work-cost-gain at one-eighth wavelength height prevented further advance. When the new type Yagi was investigated it was decided to put the extra five elements on in one big heap.

A glance at the sketches show that Fig. 1 Section A is just a typical type of 5 el. Yagi except that the reflector

spacing is 0.24 instead of 0.25. That spacing was evolved using a double wire, spaced 6 inches, for the reflector. (Changing it to a single wire landed me in strife.) Section A of Fig. 1 represents the changed Yagi via the new type spacing of 0.4 wavelength, the joining director being at spacing 0.2 wavelength, but 0.4 for this also is in order.

Fig. 2 shows how the nearest two directors and the reflector were changed over to give a 4 element beam of enough gain for skeds in VK9 land (north). This 7 MHz. beam is on a compass bearing of S from a position approx. 70 nautical miles NW from Brisbane.



FIG. 1. Section A. 5 EL. YAGI.



FIG. 1. Section B. 10 EL. LONG YAGI.

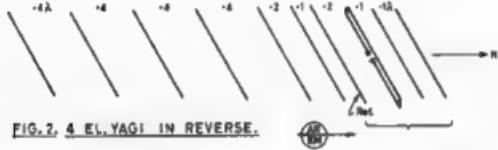


FIG. 2. 4 EL. YAGI IN REVERSE.

Of interest at this point is that the two-wire reflector represented quite a different effect on the impedance of the driven element than a single wire, or of that wire plus 12 inches. The factors concerned are that a folded dipole, if altered to the shape of a quad, could not have a director or reflector of a single wire. In this case, I had added three more elements to the 10 mentioned, but the gain was well down until I reverted to the original double wire reflector of 5% longer than the three-wire dipole.

From the above it is clear that the first five elements of the Yagi must be in order before the other elements are added. At this QTH the gain of the second group was far beyond that of the first group, but as explained previously, the QTH position absorbed the initial gain. The results were astonishing, especially at the other end where friends had spent years straining their ears in my direction. If I had any sense at all I would be sitting back enjoying the performance of this big beam. Instead of that, I exhibit my ignorance and show others how to equal in four days the results that took me four years to obtain.

As this article is aimed at helping (1) the bottom half, (2) the young, and (3) the inexperienced groups, much detail in construction work is necessary. It is hoped that the many problems mentioned will create a desire to solve them. It is quite clear that initially neither much money or knowledge is necessary for experimental work. For a genuine experimenter, assistance and sound technical advice is available at all times just by crying into the mike. Antenna design, progressing mathematically,

leaves many gaps that can be better probed by a practical organisation such as ours, but there is little encouragement for our new members when all awards go for DX, and quality is down in the doldrums. If we lift the quality of our transmission, then Amateur Radio will get a push-up instead of its customary push-down.

On 7 MHz. quality is useless unless it rides free of the QRM. It is here that beams become important because (1) of their effect on the signal-to-noise ratio, (2) their ability to restore the strength after other methods that were used to improve that ratio had reduced

styrene piping for the joins and bamboo for the top section. If home-brew type is desired, suitable boards can be sawed by nailing to an upright 3 x 2 with the required edge protruding and the saw guided by the upright. Thin poles will have to support from nylon string. Bricklayers' twisted nylon string has been used here for use on the elements. Small metal rings can act as pulleys for erecting the element wires and also for bracing the light poles.

With the pulley at its correct height, the minimum length of nylon string for raising the elements is such that you can reach both ends. Aligning the elements is tricky but it is quite easy if you use a plumb-bob (a big nut on some cotton). With the posts in position, work from the centres. Mark the centres of the elements with dark tape. Fasten to the centre peg and complete the element wiring for that approximate length to the end poles. With the centre pegs all in line raise the elements themselves. (It is advisable to join the centres of the dipole and three directors together at the right distance with nylon string.) By holding the plumb-bob up at arms length all elements can be aligned with respect to their pegs. Another method that I use is to hang a white cord from the reflector centre then from the centre peg of the furthest element align that reflector cord with a mark on the opposite hill, then advance toward it, aligning each element. Small changes are easily made on fixed elements by ramming the posts on one side.

For the "portables" some experimenting has been done. These particular measurements are only approximate. They were taken without a tape by lowering the end. The dowel used was holding up the tenth element of a Yagi beam on 7 MHz. The wire in use was 16 gauge steel, the length being 70 ft. plus about 5 ft. folded back and with two light insulators. Only the slightest of bends was observed in the 18 ft. of 5/8 inch dowel (two sections of 9 ft.). The type used was the kind popular for window curtains. 50 ft. of nylon string was also required. If you look at Fig. 4, it will show you how to get that dowel

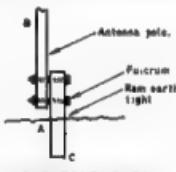


FIG. 3. POLE BASE.

up without it making figure eights. Fasten the nylon string to the top of the dowel and the wire of the element. It needs 24 ft. on each side to go to the pegs. With the dowel lying along the dotted line, follow it until the string to peg B and the element come tight. At this stage the top of the dowel will rise until the pull from the other peg (A) halts the rise. Now align the bottom for least bend in the dowel, which in this case came about 3 ft. towards the other end of the element, from the vertical position.

To join the two sections of dowel, look at Fig. 5. Again using polystyrene water pipe of 1 inch diam, cut off two sections 5 inches long. Leave A intact, cut down B for the full length and then fold it up so it will slip inside A. Now take a 6 inch length this time and cut out a section 1 inch wide down the whole length (or such a width as will enable it to fit inside the second tube). The protruding  $\frac{1}{2}$  inch at each end should have about five cuts  $\frac{1}{8}$  inch deep to let it expand for easier entry of the 5/8 inch dowels.

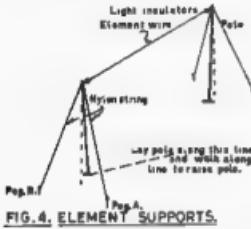


FIG. 4. ELEMENT SUPPORTS.

We come now to "spacers". Polystyrene and its class have good qualities. They are light and being 1 inch in diam. (in this case) they get over the "twisting" habit of home-brew lines. If you look at Fig. 6 it will show how to hold these slippery things while you operate on them. Fig. 7 has the holes spaced at six times the diameter of the wire for 300 ohm use—note the exact way the cut enters the hole and the side on which the nick is made. This gives a flap that can be twisted sideways to let the wires be "clipped" on.

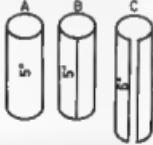


FIG. 5. DOWEL JOINERS.

If you were to extend this drawing to accommodate one more hole in the centre between the two that are already there, you would have the 3 element folded dipole that is used in this and the former beams. These spacers were strung through the centre holes for the centre wire, then spaced in a distance of a couple of feet, then the top and bottom wires were "clipped" on. Lack of space prevents me from explaining why they don't twist even after a couple of years and probably a hundred up and down trips. For your information, warm these things in the sun. They can then be cut quite easily.

Another problem is wire. Hold the coil in the left hand and after fastening one end, walk backwards peeling the coils off to the right, say five turns, then hold it in the right hand and peel off five turns on the other side. This cancels the twist.

Now to conclude. This work is not a one-man effort. Assistance has been given freely by all Amateurs called on. The main ones concerned have been

VK2BAI, of Sydney, the "Man Friday" who has spent four years (with only one break of a few months) giving band conditions, reports, etc., at 2100 hours or 2000 EAST. Also VK4LN, of Gypie, 20 miles distant, who shouldered the responsibility of keeping everything in order and also supervised the quality of the transmissions at all times. Theory and technical advice came also from VK4XR, of Gypie. The transmitter in use was a.m. with 120 watts.

Before closing I will draw your attention to a few points:

- (1) The effect of wavelength height.
- (2) The importance of the signal-to-noise ratio.
- (3) The effect of this type of Yagi on that factor if extended to a useful limit of six wavelengths of boom length (two wavelengths used here).
- (4) The signal side-rejection characteristic.
- (5) The comparison of gain in the two sections of the 10 el. Yagi, which in my case was influenced by the valley QTH position.
- (6) The fact that the same receiving station could issue one report using a receiver for a.m., another while using an a.s.b. transceiver, and a third using his guess meter. Poor old Prof. Einstein would have thought that all his efforts in writing of the need of a common "measuring stick" had been in vain.



FIG. 6. PIPE HOLDER.

A little comment is necessary on the signal-to-noise ratio as it applies to both transmit and receive. I have assumed that an antenna with a good S to N ratio will act similarly on both transmit and receive. This is based on two factors, (1) the law of reciprocity (its application to beams was quoted in a previous article I think on Rhombics), (2) on a curious report received from VK2BAI where the QRM was bashed down generally, but one distant signal was still there and came up riding in on the beam. This does not necessarily mean that we broadcast our own QRM, that question should be split up into many components.

This completes this article, but in the construction field the principles of a few items should be fully understood. For home-brew lines, for example, take three pieces of the steel wire quoted and insert them in the water pipe as described and see how the cylinder construction effects both the twist factor.



FIG. 7. LINE SPACER.

and the distance apart required. For the 18 ft. dowel of 5/8 inch diam. construction, use two pins and cotton plus a straw out of the millet broom to represent the antenna problem, and how to fix it so that the strain comes on the upright in the position where it stands it best. For the join of the two sections of dowel, 1 inch piping was used because it was available, but  $\frac{1}{2}$  inch can be purchased, also suitable conduit.

No work has been done on wavelength heights below one-eighth. I trust that others will see the possibilities in this changed type of Yagi. If it does not suit our methods, then we might alter our methods to suit it. If we look at our award system then we can come to no other conclusion than to regard Amateur Radio as a play-toy, not an experimental group.



## THE REPAIR BENCH

(continued from page 11)

either go lower or return to the infinity end of the scale.

Connect the leads for the lower reading. Of course they are between emitter and collector. The negative ohmmeter lead is at the collector. This works for NPN or PNP. Put a spot of paint or fingernail polish by the collector wire so you can identify it thereafter.

### LEAKAGE BY OHMMETER

The tests you've already made tell you if a transistor is leaky or shorted. It's just a matter of interpreting.

When you've established the two low-resistance readings from the base, notice the readings in the reverse directions. If they're under 10K for either junction, there is too much leakage.

If you find low readings in both directions between any two leads, that junction is shorted. If a reading between two leads shows open both ways, even on the Rx100K scale, that junction is open.

A reading less than 10K from collector to emitter, in either direction, indicates too much leakage.

**Two-step method for identifying a transistor type, and base, collector and emitter connections. You need only your ohmmeter, but the transistor should be out of the circuit.**

### CHARACTER TESTS

**Step 1.**—Find transistor lead that measures low R (150 ohms or less) to both other leads; that is the base lead

If the ohmmeter lead on the base goes to the . . . negative positive and of your ohmmeter battery, the transistor is . . . PNP NPN

**Step 2.**—Connect the ohmmeter for lowest R (above 10K) between the remaining transistor leads. The negative ohmmeter lead identifies the collector.

# ROSS HULL MEMORIAL VHF/UHF CONTEST, 1970-71

The Federal Contest Committee of the Wireless Institute of Australia invites all Australian and Overseas Amateurs and Short Wave Listeners to participate in this annual Contest which is held to perpetuate the memory of Ross Hull whose interest in v.h.f./u.h.f. did much to advance the art.

A Perpetual Trophy is awarded annually for competition between members of the W.I.A. in Australia and its Territories, inscribed with the name and life work of the man whom it honours. The name of the winning member of the W.I.A. each year is also inscribed on the Trophy. In addition, this member will receive a suitably inscribed certificate.

## OBJECTS

Australian Amateurs will endeavour to contact as many other Amateurs in VK Call Areas and Foreign Call Areas under the following conditions.

## DATE OF CONTEST

From 0001 hours E.A.S.T., 12th December, 1970, to 2359 hours E.A.S.T., 24th January, 1971.

## DURATION

Any seven calendar days within the dates mentioned above, not necessarily consecutive. These periods are to be at the operator's convenience. A calendar day is from 0001 hours E.A.S.T. to 2359 hours E.A.S.T.

## RULES

1. There are two divisions, one of 48 hours duration, and one for seven days. In the seven-day division, there are three sections:

- (a) Transmitting, Open.
- (b) Transmitting, Phone.
- (c) Receiving, Open.

2. All Australian and Overseas Amateurs may enter for the Contest whether their stations are fixed, portable or mobile.

3. All Amateur v.h.f./u.h.f. bands may be used, but no cross-band operating is permitted. Operators are cautioned against operating transmitting equipment on more than one frequency at a time, particularly when passing ciphers. Cross-band operation to assist contest working is prohibited.

Such operation will be grounds for disqualification. Cross mode contacts will be permitted.

4. Amateurs may enter for any of the transmitting sections. The seven-day winner is not eligible for the 48-hour award.

5. Only one contact per band per station is allowed each calendar day.

6. Only one licensed Amateur is permitted to operate any one station under the owner's call sign. Should two or more operate any particular station, each will be considered a contestant and must submit a separate log under his own call sign.

7. Entrants must operate within the terms of their licences.

8. **Ciphers:** Before points may be claimed for a contact, serial numbers must be exchanged. The serial numbers of five or six figures will be made up of the RS (telephony) or RST (e.w.) report plus three figures, commencing in the range 001 to 999, for the first contact, and will then increase in value by one for each successive contact. When a contestant reaches 999 he will then commence again with 001.

9. **Entries** must be set out as shown in the example, using only one side of the paper. Entries must be post-marked not later than 8th February, 1971, and clearly marked "Ross Hull Contest" and addressed to Federal Contest Manager, Box N1002, G.P.O., Perth, W.A. 6001.

10. **Scoring** for all sections will be based on the attached table. Approx. distances to be shown in the log entry as shown in the example. Failure to make this entry will invalidate the particular claim. **Operation via active repeaters or translators is not allowed for scoring purposes.**

11. **Logs.** All logs shall be set out as in the example and in addition will carry a summary sheet showing the following information:

Name ..... Call Sign  
Address ..... Division  
..... Claimed Score

## SCORING TABLE

Distance in Miles	52 Mc.	144 Mc.	429 Mc.	576 Mc. Higher
Up to 25 Miles	1	1	2	5 10
26 to 50	"	1	5	10 25
51 to 100	"	5	15	30 50
101 to 200	"	10	25	50 100
201 to 300	"	25	15	50 150 250
301 to 500	"	20	25	100 250 300
501 to 1000	"	10	35	200 300 350
1001 to 1500	"	15	100	250 350 400
1501 to 2500	"	25	125	300 450 500
2501 to 3500	"	35	200	400 500 600
3501 to 5000	"	50	300	450 550 650
5001 and over	"	100	400	500 600 700

## EXAMPLE OF TRANSMITTING LOG (Brisbane Station)

Date/Time E.A.S.T.	Band Mc.	Emissions Power	Call Sign	RST/No. Sent	RST/No. Recvd.	Dist. Miles	Points Claimed
24th Dec. 0000 E.A.S.T.	52	A3(a)	VK7ZAJ	59001	59004	1110	15
0010 E.A.S.T.	52	A3(a)	VK7MNG	59002	57061	330	20
0020 E.A.S.T.	144	A3	VK5ZK	56003	55043	990	35
0025 E.A.S.T.	144	A3	VK5ZQ	45004	46021	850	35

## EXAMPLE OF RECEIVING LOG (Perth S.W.J.)

Date/Time E.A.S.T.	Band Mc.	Call Received	RST/No. Sent	Station Called	Dist. Miles	Pts Claimed
2nd Jan. 0000 E.A.S.T.	52	VK5ZDX	59221	VK5KK	1330	15
0025 E.A.S.T.	52	VK5ZCF	58195	VK5ZAA	2040	25
1110 E.A.S.T.	432	VK5ZDS/6	57061	VK5LK/6	60	15
2210 E.A.S.T.	144	VK5ZHU	44102	VK5ZCN	1330	100

Operating Dates ..... (7 cal. days)  
Highest Score over a 48-hour period  
was ..... points.

Operating period:  
from hrs. E.A.S.T. / /  
to hrs. E.A.S.T. / /

**Declaration:** I hereby certify that I have operated in accordance with the conditions of my licence and abided by the Rules of the Contest.

Signed

Date

12. Entrants not abiding by the Rules of this Contest will be disqualified.

13. The ruling of the Federal Contest Committee of the W.I.A. will be final. No dispute will be entered into.

14. **Awards:** Certificates will be awarded to the winners of each section in each VK and Overseas Call Area. The VK contestant who returns the highest score in the transmitting section and who is a financial member of the W.I.A. will have his name inscribed on the Trophy which will be held by his Division for the prescribed period. A Certificate will be awarded to the contestant who shall not be the Trophy winner, and who returns the highest scoring log covering a period of any 48 consecutive hours.

Also, Certificates will be awarded for operating in the Ross Hull Contest and breaking any Australian v.h.f./u.h.f. distance record.

## RECEIVING SECTION

1. Short Wave Listeners in Australia and Overseas may enter for the Contest, but no transmitting station may enter.

2. Contest times and logging of stations on each band are as for the transmitting sections, however there is no 48 hour sub-section.

3. To count for points, logs will take the same form as for transmitting sections, but will omit the serial number received. Logs must show the call sign of the station heard (not the station worked), the serial number sent by it, and the call sign of the station being worked.

Scoring will be on the same basis as for transmitting stations, i.e. on the distance between the Listener's station and the station heard. See the examples given. It is not sufficient to log a station calling CQ.

4. A station heard may be logged only once per calendar day on each band for scoring purposes.

5. **Awards:** Certificates will be awarded to the highest scorer in VK and Overseas countries.



### Phone (continued)

VKSUC	85 Pts.	VKSCL	26 Pts.
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SLC	71 "	SZEE1	26 "
SSB	85 "	SZEE2	26 "
SZKX	85 "	SZEE3	26 "
SXY	84 "	SOT	26 "
SVT	47 "	SZELZ	21 "
SZKJ	40 "	SLG	20 "
HTV	370 "	SDUS	18 "
SZP	36 "	SDWW	18 "
SZPQ	36 "	SDY	18 "
SZRN	38 "	SCA	16 "
SZGZ	35 "	SZIS	8 "
SZPJ	30 "		
<b>C.W.</b>			
VKXMY	380 Pts.	VKSUR	44 Pts.
SOR	181 "	SNU	25 "
SBS	180 "	SAU	28 "
SMZ	166 "	STL	30 "
SLD	161 "	SKU	15 "
<b>Open</b>			
VKXJ	380 Pts.	VKSVD	309 Pts.
SEK	380 "	SEK	234 "
SAX	380 "	SEK	180 "
SIF	380 "	SGH	48 "
SOH	380 "	SJC	44 "
SVW	382 "		

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EDR	991 "	SHG	55 "
EDZK	995 "	SHR	57 "
EWY	994 "	GWX	51 "
EDZM	994 "	SHG	51 "
EAS	981 "	STK	47 "
EKK	453 "	60R	37 "
EAO	384 "	67B	35 "
EJY	362 "	62DB	35 "
EDW	359 "	SMH	35 "
ELO	354 "	6CN	35 "
SVK	354 "	6RU	22 "
SKR	280 "	6XW	22 "
STG	265 "	6PZ	21 "
EWL	262 "	6ZP	21 "
SCP	197 "	6ZPZ	15 "
SMB	183 "	6RJ	14 "
EPH	183 "	6AWI	14 "
EDC	146 "	6ZPZ	14 "
EDC	146 "	6XK	13 "
EMO	132 "	6ZAY	10 "
GNB	81 "	6ZDK	10 "
6FG	78 "	6ZFD	10 "
<b>C.W.</b>			
VKSAT	382 Pts.	VKSPL	250 Pts.
SWT	372 "	6AJ	137 "
SGI	380 "	6ZLZ	13 "
<b>Open</b>			
VK5MA	388 Pts.	VKSVB	247 Pts.
6JK	443 "	5NK	140 "
6HD	418 "	SCR	45 "
6RS	386 "		

### TASMANIA

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VKTAZ	1540 Pts.	VKTH	122 Pts.
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7ZV	1612 "	7EF	100 "
7MD	1012 "	7DZ	100 "
7WF	784 "	7LZ	74 "
7FM	886 "	7DZ	64 "
7ZK	886 "	7AB	64 "
7GC	660 "	7ZV	64 "
7UK	661 "	7KH	41 "
7LS	415 "	7RZ	39 "
7SR	335 "	7PZ	39 "
7JZ	310 "	7ZP	39 "
7MX	310 "	7ZRO	38 "
7SM	278 "	7ZPZ	38 "
7KZ	266 "	27MK	37 "
TAX	242 "	7CT	37 "
7CS	237 "	7ZAS	23 "
7ED	237 "	7ZLZ	23 "
7IL	185 "	7MK	16 "
7PS	176 "	7BQ	8 "
7MG	169 "	7ZAK	7 "
<b>C.W.</b>			
VKTCH	430 Pts.	VKTKE	135 Pts.
7LJ	306 "	7EJ	78 "
TRY	182 "		
<b>Open</b>			
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7SM	1153 "	7NC	167 "
7PF	570 "	7DM	85 "
7EE	426 "		

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1MF	71 "	1ZRH	6 "
1YR	33 "		

#### C.W.

VK1AG	5 Pts.
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#### Open

VK1BC	1112 Pts.	VK1VK	263 Pts.
1PV	942 "	1DA	183 "
1AOP	247 "		

#### C.W.

VK1AD	364 Pts.	VK1AZ	196 Pts.
2EQ	280 "		

#### Open

VK1BIC	1816 Pts.	VK1JS	308 Pts.
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### PAPUA-NEW GUINEA AND TERRITORIES

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VK5GA	1120 Pts.	VKSAG	215 Pts.
88Y	806 "	6JL	67 "
88Z	720 "	8NL	67 "
8XK	650 "	8NL	67 "
8TC	620 "	8NL	44 "
8AC	247 "	8ZC	60 "

#### Open

VK5HD	388 Pts.
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### LISTENERS' SECTION

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# NEW CALL SIGNS

JUNE 1970

**VK1YR**—Canberra Y.M.C.A. Radio Club, Station, Corroboree Park Youth Centre, Albury, Postal: 16 Bannister Gardens, Manuka, 2603.

**VK1ZPB**—P. F. Bell, 39 Larakia St., Warrnambool, 32811.

**VK1ZWG**—W. R. Godfrey, Station: 1 Gurn St., Higgins, Postal: P.O. Box 15, Blayney 2744, N.S.W., 2860.

**VK2ADY**—S. D. Hunt, 35 Mathews St., West Tamworth, 2340.

**VK2ATY**—L. W. A. Doolan, Station: Technical College, Newcastle, Postal: 130 Rae Cres., Kotara South, 2288.

**VK2BHG**—M. A. Harrison, 14 Market St., Rockdale, 2216.

**VK2BRY**—J. A. Allinson, #8 Wardell Rd., Dulwich Hill, 2210.

**VK2ZKR**—T. F. Laird, 151 Tudor St., Hamilton, 2203.

**VKE2HU**—G. B. Cuthbert, 2 Nicka Ave., Keira, 2200.

**VKE2KI**—B. R. Patterson, 30 Hyacinth St., Asquith, 2078.

**VKE2NA**—M. J. Furrell, 4/183 Hopetoun Ave., Vaucluse, 2030.

**VKE2QA**—R. J. Irving, 7 Lane Pl., Merrylands, 2160.

**VK2ZSQ**—R. J. Murray, 34 Mona St., Auburn, 2144.

**VKE2VK**—V. H. Kaasd, 33 Edna Ave., Merrylands, 2160.

**VK3AFB**—R. H. Rigler, 12 Palmerston Crt., Greenborough, 3088.

**VK3AZK**—W. D. H. Herwood, 35 South Valley Rd., Highton, 3218.

**VK3BDE**—Geelong Grammar School, Radio Club, Geelong Grammar School, Corio, 3218.

**VK3BDE**—LaTrobe University Physics Society, LaTrobe University, Bundoora, 3083.

**VK3BDF**—R. N. Field, 3 Mardon Crt., Nunawading, 3131.

**VK3BFB**—D. Williams, 25 Wentworth Ave., Sandringham, 3191.

**VK3BDO**—E. A. King-Smith, 311 Centre Rd., Bentleigh, 3204.

**VK3BDP**—J. E. Falkner, 17 Burgess St., Hawthorn, 3120.

**VK3BDW**—J. E. Wissman, 20 Austral Ave., Ferntree Gully, 3156.

**VK3BET**—E. E. Tilley, 10 Tudor Crt., North Balwyn, 3104.

**VK3BFL**—T. H. M. Chittock, 11 Lt. Myers St., Geelong, 3220.

**VK3CCG**—R. Hooper, Portable/Mobile.

**VK3CV**—N. R. Leidlaw, 43 Churchill Ave., Bendigo, 3550.

**VK3VDG**—G. J. Gill, 19 Dorset Rd., Croydon, 3136.

**VK3YDH**—A. N. Campbell, 30 Campbell St., Coburg, 3056.

**VK3YDM**—C. J. Jarvis, 9/105 Willenden Rd., Oakleigh, 3165.

**VK3YDP**—T. J. Alder, 26 Gramatan Ave., Beaumaris, 3183.

**VK3YDQ**—G. R. H. Vreland, "Cartercra," Strathbogie, 3665.

**VK3YDV**—S. P. Pritchard, 22 Holland Rd., Blackburn South, 3130.

**VK3YDY**—K. W. Forbes, 7 Rooney St., Moorabbin, 3159.

**VK3YDZ**—K. E. Lewis, "Kanda," Boes Rd., Nunawading, 3136.

**VK3YDZ**—C. Maloney, Belconnen, Jersey Stud, Tongala, 3631.

**VKE2ZB**—R. J. Beever, 11th St., Mildura, 3500.

**VK3ZDD**—M. J. Dow, 105 Bayview St., Wilmot, 3618.

**VK3ZDZ**—J. F. Davis, Lot 10, Cousin Dr., Baywater, 3133.

**VK4NT**—N. T. Casey, 33 Herberton St., Maribyrnong, 3880.

**VK4SZ**—Sunshine Coast Amateur Radio Club, 201, 7 Bannister Ave., Nambour, 4560. Postal: C/o. Radio Station 4NA, P.O. Box 279, Nambour, 4560.

**VK4ZJ**—R. J. Webb, 151 Alderley St., Toowong, 3200.

**VK4ZK**—A. J. McLean, Station: Mobile, Postal: C/o. Newmarket Gardens Carevan Park, 199 Ashgrove Rd., Ashgrove, 4060.

**VK4ZLB**—R. R. Hartwig, Bona Vista Ave., Bonnall, 4310.

**VK4ZLB**—R. S. Best, 12 Ardyne Rd., Corinderra, 4073.

**VK4ZLG**—A. W. Reynolds, 159 The Esplanade, Cairns, 4870.

**VK4ZLJ**—I. S. Graham, Station: Dakenber Rd., Mt. Murchison, Postal: P.O. Box 567, Biloela, 4715.

**VK4ZLJ**—A. J. Andrews, 151 Gailey Rd., Tewantin, 4568.

**VK4ZKP**—K. R. Pollock, 80 Vernon St., Nunawading, 3131.

**VK4ZLJ**—R. Woods, 23 Stanley St., Inglewood, 3200.

**VK4ZLZ**—S. D. Doherty, Station: Manic Rd., Thangool, 4716. Postal: P.O. Box 16, Thangool, 4716.

**VK5AE**—A. M. Park, 10 Vine St., Morphett Vale, 5162.

**VK5AU**—R. W. K. Adams, O.T.C. (A) Staff Quarters, Lambeth St., Ceduna, 5860.

**VK5BW**—C. R. Norman, The Parkway, Paradise, 3075.

**VK5XJ**—A. J. Hannaford, 2/38 Broughton St., Clandeboye, 5053.

**VKA2ZP**—T. P. E. McMahon, 36 Creekview Dr., Redwood Park, 5007.

**VK5ZPG**—P. G. Whelum, 8 Coronation Pl., Port Lincoln, 5600.

**VK5ZQ**—W. J. Stevens, Station: Section 45, Hundred of Yednarie, Postal: P.O. Box 70, Cleve, 5640.

**VK5ZXD**—J. J. Pitchfork, 15 Brigalow Ave., Seaccombe Gardens, 5047.

**VK6AB**—T. K. C. Blacknell, 48 Sanderson St., Leamington, 8078.

**VK6AZ**—G. P. Clifton, 13 Morley Dr., Morley, 6065.

**VK6EK**—A. E. King, 4 Mario Rd., Greenmount, 6056.

**VK6ZAT**—R. A. Taylor, 118 Broome St., Highgate Hill, 3068.

**VK6ZB**—G. B. Burlinson, Station: Portable, Postal: C/o. B.H.P. Exploration Party, P.M. B. Kalgroote, 6430.

**VK6ZEG**—P. D. Morgan, 88 Clayton St., Bellavue, 6036.

**VK7AR**—H. Young, 1 Medder Pl., Devonport, 7910.

**VK7EJ**—L. E. Eadie, 16A Stoke St., New Town, 7008.

**VK7TH**—H. J. Hoek, 363 Nelson Rd., Mt. Nelson, 7007.

**VK8AJ**—F. J. Scougall, 13 Achilpa St., Alice Springs, 0870.

**VK8ZRM**—R. J. Maginnis, 36 Gregory St., Paspa, 4860.

**VK9AG**—A. G. Nunn, Station: Walangana Rd., Rahaui, N.G., Postal: P.O. Box 10, Rahaui, N.G.

**VK9AV**—E. V. Avenell, St. Michael's Estate Kletta, Rougaville, N.G.

## CANCELLATIONS

**VK3AQP**—J. H. L. Field, Transferred to Vlo.

**VK3ATJ**—P. H. Crowe, Not renewed.

**VK3ZL**—R. J. Webb, Not renewed.

**VK3ZP**—R. J. Webb, Now VK3ATY.

**VK3ZPB**—P. F. Bell, Now VK3ZP.

**VK3DJ**—J. L. Gleeson, Not renewed.

**VK3EW**—E. C. Wheeler, Deceased.

**VK3GX**—P. R. Gibson, Deceased.

**VK3HY**—F. E. Trutmann, Not renewed.

**VK3JX**—R. Family, Deceased.

**VK3NZ**—J. D. T. T. Not renewed.

**VK3AH1**—Vogel, Not renewed.

**VK3AJK**—J. Spark, Not renewed.

**VK3ASY**—O. W. Guy, Not renewed.

**VK3AXT**—R. S. Davies, Not renewed.

**VK3AZM**—J. Adams, Station: Now VK5BU.

**VK3ZB**—J. A. Reichard, Not renewed.

**VK3ZPQ**—K. M. Cocking, Not renewed.

**VK3ZIR**—D. R. Rigler, Now VK3AFB.

**VK3ZK**—D. R. Chittock, Now VK3EFL/T.

**VK3ZLW**—R. M. S. Slock, Not renewed.

**VK3ZT**—C. Qualin, Not renewed.

**VK3ZTJ**—V. Aviley, Not renewed.

**VK3ZVA**—R. D. Young, Not renewed.

**VK4VQ**—E. V. Avenell, Now VK9AV.

**VK4WJ**—R. J. Webb, Now VK4ZJ.

**VK5BZ**—C. H. Bassey, Deceased.

**VK5EN**—T. A. R. E. Nitschke, Not renewed.

**VK5ZWS**—J. B. Sparrow, Deceased.

**VK6ZCB**—T. K. C. Blacknell, Now VK9AB/T.

**VK6ZDV**—D. E. King, Now VK6EK.

**VK7ZB**—H. Young, Now VK7AR.

**VK7ZED**—J. L. Eadie, Now VK7IE.

**VK7ZEK**—W. I. Hoek, Now VK7TH.

**VK8AX**—B. Hannaford, Now VK8CI.

**VK9DS**—B. W. Smeaton, Not renewed.

**VK9TB**—E. W. Bastow, Not renewed.

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AND A 1296 MHZ. CONVERTER

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★ **"73"** Magazine, \$5.50; Three Years, \$11.50.

★ **"Ham Radio"** Magazine, \$5.50; Three Years, \$11.50.

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# MAILING OF QSL CARDS

Dear Sir,

Some time ago I decided to write to the P.M.G. Department on the question of postal charges and classification of QSL cards in unsealed envelopes for the purpose of direct QSL'ing.

I feel this may be of some interest to other Amateurs, who on occasions prefer to QSL direct, and who may have been in some doubt as to the relevant class and postal charges. This arose as I had received several cards in unsealed envelopes, marked "2nd class airmail" and on one occasion "printed matter only". Obviously there was a marked difference in postal charges.

Here then, is the reply from the P.M.G. Department.

—Peter F. Morrow, AX2BMP.

\* \* \*

Postmaster-General's Dept.,  
Sydney Mail Exchange,  
N.S.W. 2012

3rd Sept., 1970

Dear Mr. Morrow,

First, may I apologise for the delay in replying to your letter of 12th August, 1970.

Following acceptance by the Universal Postal Union of a proposal designed to abolish commercial papers as a separate category, articles originally considered as commercial papers are now classified as letter post except the following, which may be transmitted at printed paper rates:

- (a) Letter post items exchanged between pupils of schools provided they are sent through school principals;
- (b) Pupils' exercises in the original or with corrections;
- (c) Manuscripts of works or for newspapers; and
- (d) Musical scores or sheets of music in manuscript.

Consequently, there is no advantage in you sending your QSL cards in unsealed envelopes as they are not eligible for the cheaper rate of postage.

Postcards cannot be posted in an envelope or wrapper so there is no alternative here.

I cannot arbitrate, of course, upon the practices in other countries. However, Universal Postal Union ruling should impose similar treatment by all member countries.

Thank you for your interesting query and if you could arrange wider publicity for the official ruling, all to the good.

—J. Saunders, for Manager,  
Sydney Mail Exchange.

## TECHNICAL ARTICLES

Readers are requested to submit articles for publication in "A.R.", in particular constructional articles, photographs of stations and gear, together with articles suitable for beginners, are required.

# Overseas Magazine Review

Compiled by Syd Clark, VK1ASC

## "HAM RADIO"

July 1970—

**Inductively Tuned High Frequency Tank Circuits.** W6SAL. High efficiency operation of parallel 3-1000Zs in the 14-16 MHz. region.

**A Variable Band State Receiver.** W1PLJ. Tunable IF on 80 meters with converters for the higher frequency bands.

**Compact Frequency Counter.** K4KRU. IC unit to count to 10 MHz. Lengthy and detailed article. Pictures included.

**Low Cost Electronic Linear for Two Meters.** K0HNN. Uses a SX1500A in a stripline circuit.

**Computer Processing Slow Scan Televisions Pictures.** W4UJMP.

**New Ideas in Telephones.** W6JTT. Seems that the old electro-mechanical machines are giving way to all electronic systems which are considerably faster.

**A Solid State H.F. Signal Generator.** VESPF. Decade frequency unit with attenuator covering the range 0.12 to 80 MHz.

**Temperature Alarms for High Power Amplifiers.** W2EZY. Since overheating is one of the first indications of a malfunction, such alarms will sound off or shut equipment down before serious damage occurs.

**SCR Regulated Power Supplies.** W4QQC. The theory and practice.

**Microwave Hybrids and Couplers for Amateurs Use.** W2CTK. Illustrates how the a.h.f. boys can roll their own instead of paying lots of money for them.

August 1970—

**Interdigital Pre-amplifier and Combline Band-pass Filter.** W8KHT. High performance filter-pre-amplifier for a.h.f. receivers that features low noise, low noise and excellent unwanted signal rejection.

**Practical VFO Design.** K5BJJ. An interesting approach to frequency stability in oscillator circuits.

**Time Frequency Counter.** K4KRU. Describes an accessory that will increase the range of your frequency counter by a factor of ten. With this unit and the counter described in this issue of 1970 you can count crystals to over 100 MHz.

**Computer Aided Circuit Analysis.** K10RY. A powerful tool that eliminates trial and error in circuit design.

**A Teamless Audio Filter for C.W.** W4JZM. Using the Maytheon 3000 linear integrated operational amplifiers, the 3 dB bandwidth is about 140 Hz.

**A VFO for Solid State Transmitters.** W3QBO. If you are tired of being rockbound here is a remarkable new VFO. It uses two MF1102 FETs and two MF1052 bipolar transistors.

**An Improved Six Metre Converter.** K10ZT. A new approach to h.f. converters using FETs and a simple local oscillator.

**Improving the Intelligibility of Communications Receivers.** WASRAQ. This author points out that sometimes the amplifier is better than the reproducer and that improvements can be made simply by improving this fellow.

**Q-Code Antennas.** K4OPZ. The performance one obtains from any antenna is almost always determined by the final adjustments made upon the unit. This author does not agree with all that has been written. Who is right?

**Modular Modules.** W8IEK. Mother and daughter printed circuit boards are used to increase IC counter circuit versatility.

## "RADIO COMMUNICATION"

June 1970—

This month's issue of the journal of the Radio Society of Great Britain contains a number of interesting articles.

**A Keyer for GREYVAL.** G3MMQ. An electronic keyer for the new moving part keying relay ideal for keying beacon stations.

**Brussels down the Brain.** G3ON. This author points out that readings obtained on the usual type of a.m.r. meter are often optimistic and even though you may have a low a.m.r. one is not always so.

**A Quarter Wave Length Vertical Aerial.** G3SSA. The British is often said to be one who hides his light under a bushel, or to put it another way, is well effacing. This Amateur has a vertical alongside the brickwork of his house.

**Technical Topics.** G3VA. Deals with "The Double Balanced Mixer," "FET Mixers," "Balanced FET converter," "All Transistor Transmitters" including some mention of VK1IGC, "Amateur Radio" and "The Australian ZEB." Modulation using transistors is also covered.

**Put a Transistor in Your Cathode.** G3SSA continues his article on getting something for almost nothing. Of course this technique has been used before to power the low power front-end of a communications receiver undergoing modification to a solid state on a stage by stage basis.

**T.V.I. Tips.** G3JGO. For those plagued by the stuff.

**Unleashing a Hopeful Future.** G3UM. Sixteenth V.h.f./U.h.f. Convention report.

July 1970—

**A 100 M. Linear using High Voltage Transistors.** G3UWF. Describes some of the possible tricks for increasing power to transistor rigs.

**A Novel Band F.M. Extender for the V.h.f. Bands.** G3JGO.

**Put a Transistor in Your Cathode.** G3SSA. A hybrid driver stage for an a.s.b. transmitter. Technical Paper.

**Technical Paper.** G3VA. This is a monthly feature conducted by the Ham Radio Association and provides a précis of a number of articles which have appeared in the various journals, not necessarily Amateur, but which appears to be of interest to a goodly number of the fraternity.

**How to Make a Good Solid State Receiver Performance.** G3JGO. With a title like that, what else can one say?

**Solid State Modules.** 2 M. Converter.

**G3GNG and G3JGO.** Noise factor better than 2 dB.

**Gain 20 dB.** D.c. supply 15-18 volts, I.c. is available: 4-dB or 25-30 MHz.

**The Deshield.** G3EWF. The newcomer to electronics usually has difficulty in understanding the dB. It is explained here once again for those who need it.

## "RADIO 2S"

June 1970—

**A Farfetched Fairy Tale.** W1JBQ. Electronic Time Meter for the Darkroom, by ZS1RA.

**About Making H.v.l. Repairs.** ZS1RR.

**Six Metre Conversion of the R-44 Transmitter.** W1JBQ. The R-44 transmitter was originally operated in the range 50-55 MHz. on three pre-set crystal controlled channels.

**Improvements for the FL1000.** S.S.B. Transmitter.

**ZS1CK.** This author states that his unit is very unstable and he found it nearly impossible to improve it until he had a major surgery. He therefore built an outboard v.f.o. and made certain other mods to improve the performance.

July 1970—

**Some Linear Considerations.** ZS3MF. A discussion of what happens if a "linear" is not how to make it so.

**Q-Codes.** Tells you what these three letter group mean.

**The 10 MHz Triband Single Feed Quad.** D. M. All Hams Are Braggins. ZS1ACD. Perhaps we are all braggarts in certain directions.

**F.M.C. The Flying Ham Club.**

## "73"

July 1970—

**An Improved Method for the Transmission of Morse Information by Slow Scan Television.** W4UJMP. Those who are interested in colour televisions, follow up on this one for them.

**World-Wide L.T.E. Prefix/Call Area List.** W1WVW. What is it?

**The Super Ante-Patch.** K3MVW. When disaster strikes there is no substitute for rapid traffic handling. This facilitates person to person contact.

**New to Build a Keyer (and relay your appearance operator status).** W4KQX. VFOs would probably find that 2000 type relays provided the necessary parts.

**A Two-Channel Starch and Lock for F.M.** W3EBC. The G3DDY rig. This simple gadget turns a two-channel rig into a single channel transmitter and provides the added capability of locking on a channel where activity is sensed.

**A Look at Allied's Portable F.M. Receivers.** K3TH. These Japanese units were made for the mobile market but can cover a wide area. They are considered to be good value although not really hot.

**450 MHz. Mighty Mite.** K3VX. Maybe one should try the British transmitter.

**Cheaper Antennas.** H. Hallen. K1CLL runs 500 watts to a pair of 81A.

**High Performance Power Supply using an IC Regulator.** K3ECP/L. Move over voltage regulation.

**Latitude Island DX-pedition.** SP3LXV and SP3KX. Good hammering holiday.



## MEET THE OTHER MAN



Ross VK4RD

Meet Ross VK4RD, ex-VK4ZRV, of Ayr, 50 miles south of Townsville in North Queensland. First licensed in 1960, Ross operates in the 88 and 144 MHz bands, plus 1440 and 2140 metres. On 88 MHz, he runs 400 watts p.e.p. s.s.b. using a 2-402Z. The converter and tunable Yagi up to 400Z. The converter and tunable Yagi, together are an SB-110A Heathkit, and he has worked VK1, 2, 3, 4, 5, 6, 7, 8, 9 and 21. (This is all except most others have worked ZL1, 2 and 3 but no 4). In addition he has worked all JAI to JA0 inclusive and KRM.

On 144 MHz, Ross runs 10 watts to a 2T15 with a 10 element Yagi up 40 feet, with an R.T.V. & H. converter to a KW17. He has not worked out of VK4 as far, and being about 900 to 1,000 miles from the main centre of metropolitan areas, he has not worked VK4 as much. His location is 12 feet above sea level. However, when the occasion permits or conditions demand, Ross is able to go out portable and has a site about 10 miles south of Ayr 600 feet above sea level, where a few more stations can be copied. Power is from a 300 watt a.c. alternator and uses the SB-110A equipment on 8 metres and 1440 transmitter and converter on 8 metres, 5 element beam for 8, 10 element for 2 metres.

Ross is a member of the W.L.A. President of Townsville Radio Club for two years, and an electrician by occupation. He has recently returned from a trip to Japan, Taiwan and Hong Kong with his brother Dale VK4ZDG and Peter VK4ZPL. They met about six VK 6 metre operators and were given a "royal" welcome. The group also visited with VK4RD, who runs 400 watts p.e.p. s.s.b. on 3 metres, then on to 2 metres fm. mobile, and the distant future 432 MHz.



Doug VK4KK

Now we go to a fresh State and get some news from Doug McArthur, of 9 Bulbul St., Ludmilla, Darwin, under the call sign of VK4KKK previously VK5KK. First "Pip" in VK4KKK, Doug has been a very keen v.h.f. type ever since. He was a former President of the VK5 V.h.f. Group, and when his work as a shift supervising technician with the Radio Australia booster station took him to Darwin, Doug's interest in amateur radio was born, and has not since been lost. He made his presence known by spending some time as President of the Darwin Radio Club. His location is 400 feet above sea level, and he holds certificates for V.H.F.C.C. and W.W. Awards. He is a member of VK5. Other interesting details re VK4KKK were given in the V.h.f. Notes for October. Taken overall, Doug might lead a very busy life, so I am sure we all wish him well in the cause of Amateur Radio.



Geoff VK6DA

Geoff VK6DA photographed at his QTH in the New Territories of Hong Kong, holding a QSL from Doug VK4KKK which records their 6 metre two-way—believed to be the first ever Hong Kong/Darwin—contact on 98 MHz.

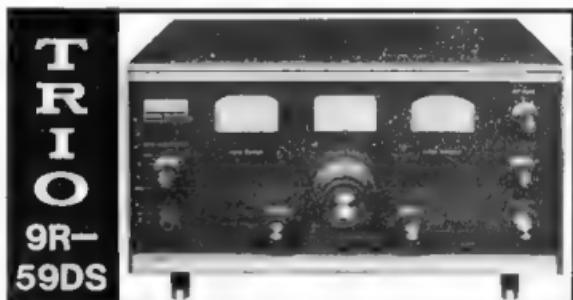
The QSO took place on 2nd June, 1970, at 1145 GMT, and was perfect 5 x 9 copy at both ends. VK6DA's 6 metre gear is on the left of the photograph in the Yards FT1460, in conjunction with the PLDX400. The beam is a 9 element wide spaced by Marconi, whilst Doug uses a home-brew transverter into an FTDX400 with a 9 element Yagi.

Geoff lives permanently in Hong Kong and is a pilot for an airline based there. He flies into Perth, W.A., from time to time and enjoys eyeballing with the VK6s. You will find him on 14.180 MHz when he's not on duty, ready to try for more VK DX on 6 metres.



John VK8ZCW with Geoff VK6DA

John VK8ZCW (on the left) with Geoff VK6DA at his QTH overlooking the sea in the New Territories of Hong Kong. The 8 metre antenna shown is the one used in the recent two-way QSO between Darwin (VK4KKK) and Hong Kong. John was able to call on Geoff recently whilst vacationing in the Far East and deliver personally the 8 metre QSL card from VK4KKK.



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## COOK BI-CENTENARY AWARD

The following additional stations have qualified for the Award:

Cert. No.	Call	Cert. No.	Call	Cert. No.	Call
554	YV1YC	622	X4KHP	680	XSYRV
655	YV1YD	623	WASZRB	681	AX2ASV
556	YV1YF	624	ZK2JAZ	682	ZK2JAZ
557	WJ1HO	625	W3HJF	683	ZL2AOA
558	G3PPP	626	W7VRO	684	HASDA
559	VE2ZED	627	AX4QA	685	GH4YJ
560	G3EFP	628	W2CDC	686	ZM2JANA
561	W1BOLG	629	W3WWS	687	PE2JZT
562	VE2TL	630	W9KFL	688	PE2LQY
563	W1QZI	631	AX3KD	689	AX2ACD
564	EP1HL	632	G3HSE	690	W7VXG
565	W1QZG	633	AX3AL	691	AX3LC
566	W1QZG	634	ZK2JZ	692	ZK2JZ
567	AX2OW	635	W8KDK	693	W7VCR
568	ZM2GJS	636	KL2DNE	694	GH4YF
569	D2K2MO	637	AX3AFA	695	MP4BHL
570	AX2AAO	638	AX3ZK	696	K1QZB
571	AX2AEC	639	AX3ZK	697	AX2ZUN
572	W1QZJ	640	SH4ZC	698	W1BQJO
573	W2BCKM	641	AX3ARQ	699	V8SAB
574	W6UWP	642	AX4EZ	700	AX3AR
575	W4AXE	643	AX3AHP	701	GH4PF
576	W1QZK	644	W7VCR	702	ZK2JPM
577	DJOKS	645	AX3AS	703	ZK2JUP
578	G3EJN/M	646	AX3RJ	704	GH4YV
579	AX2XW	647	W8AEDC	705	W8TSUH
580	JAGLTU	648	KL7GSC	706	V7EBBP
581	AX2ZC	649	W7VCR	707	W7VCR
582	W1QZT	650	W5BDMN	708	W7VCR
583	W2BCKM	651	DJ4P1	709	W7VCR
584	W1QZK	652	AX4GG	710	W8ASRAS
585	WAFTND	653	AX3YC	711	V8EAS
586	W1QZK	654	AX3ZK	712	W8ASR
587	W1QZP	655	W8ACG	713	W8ASR
588	LU2AQ	656	AX3AMA	714	W8ASR
589	GS2KA	657	AX4FE	715	W8ASR
590	EL2SC	658	AX3EKR	716	W8ASR
591	W1QZP	659	W7VCR	717	W8ASR
592	W1QZP	660	GH4PF	718	W8ASR
593	W4VHY	661	SG1OT	719	AX4TT
594	W3CJF	662	AX2AL	720	K8VQG
595	W2BKL	663	AX6DR	721	VE4A
596	W1QZQ	664	W8ACG	722	W8ASR
597	W1QZQ	665	W8ASR	723	W8ASR
598	W2BKL	666	AX3BDH	724	W8ASR
599	KOBLT	667	Q3IDW	725	W8ASR
600	KB2PY	668	W8B4MK	726	W8ASR
601	W2COC	669	W7VCR	727	W8ASR
602	W1QZP	670	GH4PF	728	W8ASR
603	W6VYV	671	AX3GA	729	W8ASR
604	XE1ER	672	W7VCR	730	W8ASR
605	W2PFL	673	W8A2Q	731	W8ASR
606	KADCR	674	AX4TT	732	W8ASR
607	W8BHQ	675	VE3BSR	733	W8ASR
608	W2BKL	676	GH4PF	734	W8ASR
609	W1QZQ	677	CT1LN	735	W8ASR
610	HB2AAA	678	AX3BBC	736	W8ASR
611	W1QZP	679	AX3V	737	W8ASR
612	W1QZP	680	AX4XK	738	W8ASR
613	BOX	681	W7VCR	739	W8ASR
614	W1QZP	682	W4WVG	740	W8ASR
615	W1QZP	683	AX3XO	741	W8ASR
616	W1QZP	684	VE3BSR	742	W8ASR
617	W1QZP	685	AX3BDH	743	W8ASR
618	W1QZP	686	AX3ZK	744	W8ASR
619	W1QZP	687	AX4MW	745	W8ASR
620	W6VZW	688	KU2PZ	746	W8ASR
621	ZM1AMQ	689	W8E2U	747	W8ASR
622	W1QZP	690	W3CKH	748	W8ASR

## COOK BI-CENTENARY AWARD

### V.H.F./U.H.F. SECTION

The following stations have qualified for the Award:

Cert. No.	Call
1	AX3ZJN
2	AX5ZBT
3	AX4ZAL

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## Correspondence

Any opinion expressed under this heading is the individual opinion of the writer and does not necessarily coincide with that of the Publishers.

### TO MALTESE EMIGRANTS

2014 Craigie Drive, Windsor, Ontario, Canada.

Editor "A.R." Dear Sir.

A large number of Maltese emigrants settled in Australia during the last 25 years. The Maltese Amateur Radio International Society is now being formed and is looking for Maltese members in every part of the world. With a population of over 160,000 Maltese Australians I am sure that a number of these are either Ham's or will be interested in knowing that the M.A.R.I.S. is now being formed.

I would like to help by giving to some space in your Federal magazine "Amateur Radio" which goes to every affiliated club in Australia and to about 4,300 Hams across the country.

We are pleased to select the Directors in the early part of next year and we are hoping to have a Director from each continent. We are now setting up the by-laws, frequency of meetings, affiliations with various wireless bodies, etc. and have prepared three colour QSL cards which will be available at a very reasonable cost to all members.

Thanking you in advance, and hoping that the responses will be great, for further information anyone can write to me at the above address.

—G. N. Muscat, Founder/Director.

[Licences are available to all naturalised migrants.—Ed.]

## W.I.A. D.X.C.C.

Listed below are the highest twelve members in each section. Position in the list is determined by the first number shown. The first number represents the total D.X.C.C. credits given, including credits given for deleted countries. The second number shown represents the total D.X.C.C. credits given, including deleted countries. Where totals are the same, listings will be alphabetical by callsign.

Credits for new members and those whose totals have been amended are also shown.

### PHONE

VK5MS	316/316	VK1AB	287/314
VK6RJ	314/338	VK4PF	287/307
VK4HR	313/333	VK4TY	284/308
VK4HO	311/328	VK3APK	281/287
VK5MK	312/323	VK3APK	281/277
VK4IKS	300/315	VK1STL	271/277
Amendments:			
VK4UC	237/237	VK4RJF	185/185
VK4PK	234/234	VK1ZL	177/177
VK3AMK	226/226	VK4AGH	113/134

### New Members:

Cert. No.	Call	Total
111	VK4HCK	137/138
112	VK4FHS	143/150
113	VK4ZK/8	104/104
114	VK3AMU	98/103

### C.W.

VK3ANQ	316/315	VK3YL	276/283
VK3QL	320/322	VK3NC	274/280
VK4FJ	290/315	VK3XBR	270/287
VK4HR	228/311	VK3ARX	270/279
VK2AGH	222/288	VK3RR	265/289
VK3APK	280/388	VK3TY	276/272
Amendments:			
VK4RP	180/177	VK4PK	186/190
OPEN:			
VK4HLR	315/314	VK4MKM	324/324
VK6RJ	310/340	VK3ZQ	320/325
VK2AHH	214/324	VK3S	301/325
VK3TY	295/329	VK3APK	301/325
VK4SD	206/321	VK4PF	286/323
VK4TY	206/321	VK3ARX	277/306

### Amendments:

VK4UC	271/272	VK4RP	326/342
VK4PK	245/250	VK4HJD	154/154
VK1ZL	250/250	VK3QK	121/121
New Members:			
Cert. No.	Call	Total	
126	VK6HSD	113/112	
127	VK6KK	148/151	
128	VK4PH	163/172	
129	VK3PA	104/112	

## MORE MISSING NAMES

Editor "A.R." Dear Sir.

The No. 4 person in the photograph is myself and I was owner and operator of station 2AD at Walton Crescent, Abbotsford Point, N.S.W. wavelength 220 metres.

I believe that the person in the front row was Mr. C. P. Bartholomew, he was President of the Wireless Institute of N.S.W. and also a Director of Amalgamated Wireless Australia Ltd. as well as a Director of Beard Watson & Co. Ltd.

Suggest that No. 8 person in the back row was Sid Colville, of Colville & Moore Radio Supplies, Rowe Street, Sydney.

—Harold R. Gregory

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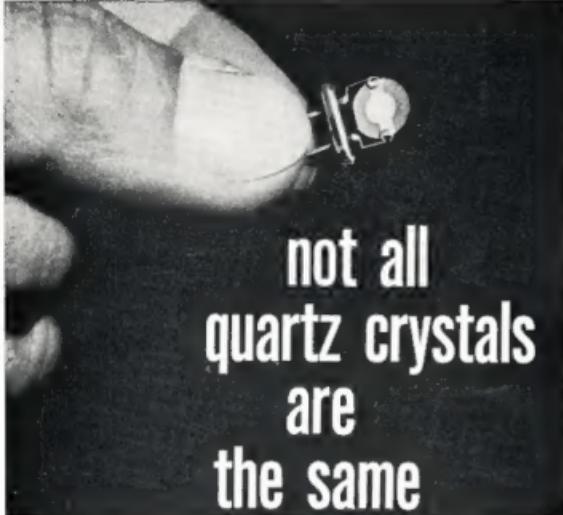
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